

Geotechnical Investigation

3/144 Dunns Crossing Road Rolleston Christchurch

> Submitted to: Hughes Developments Ltd Christchurch



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14.08.2020 12903.001.000_91

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ENGEO Document Control:

Report Title	Geotechnical Investigation - 3/144	eotechnical Investigation - 3/144 Dunns Crossing Road, Rolleston											
Project No.	12903.001.000	91	91										
Client	Hughes Developments Ltd	Client Contact	<										
Distribution (PDF)	Kelvin Back												
Date	Revision Details/Status	WP	Author	Reviewer									
14/08/2020	Issued to Client	JT	JRW	GM									



1 Introduction

ENGEO Ltd was requested by Hughes Developments Ltd to undertake a geotechnical investigation of the property at 3/144 Dunns Crossing Road, Rolleston, Christchurch, as outlined in our variation proposal (ref: P2020.004.581_01).

The purpose of this assessment was to conceptualise a geological model of the site, assess the likely future land performance, comment on the suitability of the site for residential subdivision, address the requirements of Section 106 of the Resource Management Act (RMA) and provide recommendations for subdivision works and foundations for typical timber framed residential dwellings.

Our scope of works included the following:

- Complete a desktop study of relevant available geotechnical and geological publications, including the NZ Geotechnical and Environment Canterbury Databases;
- Undertake a geotechnical site walkover;
- Undertake five hand auger boreholes with associated Scala penetrometer tests to assess the near surface material types and strength characteristics;
- Organise and technically supervise the excavation of six test pits, including geotechnical logging of the exposed soils; and
- Preparation of this report outlining our findings on the ground conditions and the suitability of the site for residential subdivision, including geotechnical advice on the likely foundation Technical Category, conceptual foundation recommendations for typical timber framed residential dwellings, and address likely geohazards as required by Section 106 of the RMA.

2 Site Description

The site comprises of one property with a total area of four hectares and the following legal description (Canterbury Maps):

• Lot 3 DP 70352 BLK III

The site is located approximately 3 km southwest of Rolleston town centre and is bound on all sides by rural properties (Figure 1).





Figure 1: Site Location Plan

Images sourced from Canterbury Maps and "© OpenStreetMap contributors". Not to scale.

3 Geological Model

3.1 Regional Geology

The site has been regionally mapped by GNS (Forsyth et al., 2008) as being underlain by brownish grey river alluvium (Q2a).



3.2 Geomorphology

The site comprises relatively flat ground, with gentle undulations and depressions in some areas. As evident on aerial imagery (Canterbury Maps, 2019) and observed during our site walkover conducted on 5 August 2020, undulating and depressed ground can be attributed to paleo-channels, which traverse the site in a general northwest to southeast direction (Figure 2). Based on observations, sandy silt deposits with variable thickness are expected to have in-filled the paleo-channels where they have not remained as channel features. Inferred paleo-channels have been mapped to give an indication of areas with potential channel in-fill (Appendix 1).



Figure 2: Historical Aerial Photo – 1990 - 1994

Image sourced from Canterbury Maps. Not to scale.

3.3 Geohazards

3.3.1 Seismicity

There are no known or mapped faults in the immediate area of the site, however the site may be at risk of ground shaking induced by movement of proximal or distal faults.

The site is located between two recently discovered fault systems, the Greendale Fault and the Port Hills Fault, the ruptures of which initiated the ongoing Canterbury Earthquake Sequence (CES). The Greendale Fault has been mapped approximately 6 km north / northwest of the site and trends roughly east-west with a surface rupture length of approximately 28 km (GNS, 2015), while the Port Hills Fault remains unmapped as the fault did not rupture at the surface. Movement on the Port Hills Fault is believed to have extended to within 1 km to 2 km below ground surface.



Large regional areas of faulting (GNS, 2015) namely the Ashley Fault, Porters Pass - Amberley Fault Zone, and the Hope and Alpine Faults, are further afield but present a high seismic hazard to the Christchurch area due to the anticipated size of earthquakes generated. The largest of these faults is the Alpine Fault, which has a return period of 250 - 300 years and is expected to produce a M8 earthquake. The last rupture on the Alpine Fault is believed to have occurred in 1717 (Pettinga et al., 2001).

3.3.2 Liquefaction and Lateral Spreading

The site is located in an area mapped where "damaging liquefaction is unlikely" (NZGD Map CGD5140, 2012), and a "zone of very low liquefaction potential" (GNS, 2006).

3.4 Site Investigation

Site investigations to assess the shallow subsurface material types and strength characteristics were undertaken by ENGEO on 7 August 2020. Six test pits and five hand auger investigations with associated Scala Penetrometer tests were completed to a maximum depth of 2.3 m below ground level.

The investigations revealed subsurface conditions across the site are consistent with the published geological mapping, as summarised in Table 1. Hand auger and test pit logs are attached as Appendix 2 of this report.

Soil Type	Depth to Top of Layer (m)	General Layer Thickness (m)	Density / Consistency	Additional Comments
TOPSOIL	0.0	0.1 – 0.3	Stiff to Very Stiff	-
Sandy GRAVEL	0.3	Unknown	Medium Dense to Very Dense	Tightly packed and consistent across the site. A thin lens of loosely packed fine to medium gravel was encountered at approximately 1 m depth across the test pit locations.

Table 1: Summary of Subsurface Investigations

3.5 ECan Boreholes

A review of six deep ECan borehole logs was conducted. The first (M36/4449 & M36/4387), are located on-site, and appear to be water wells providing the properties irrigation and domestic supply. The other boreholes are located to the north (M36/4450), east (M36/20535), south (BX23/0895) and west (M36/7416) of the site.

Well logs from the six holes of interest are attached to this report as Appendix 3 and summarised in Table 2.



ECan Borehole	Total Depth (m)	Water Level Below Ground Level (m)	Generalised Borelog as Logged by Driller
M36/5041	34	9.73	Gravel with silt and sand to 34 m depth.
M36/0016	15.2	9.85	Sandy gravel to 15.2 m depth.
M36/5042	32.5	9.97	Sandy gravel to 32.5 m depth.
M36/5038	32	9.58	Sandy gravel to 32 m depth.

Table 2: Generalised Summary of ECan Boreholes

Figure 3: Nearby ECan Borehole Locations



Aerial photograph sourced from Canterbury Maps. Not to scale.



3.6 Groundwater

Groundwater is recorded in the surrounding boreholes between approximately 9 to 10 m depth.

3.7 Site Seismic Class

In accordance with NZS 1170.5:2004, Class D applies to this particular site, defining it as a 'deep soft soil site'.

4 Liquefaction Analysis

Owing to the nature of the subsurface materials and depth to groundwater at the site, we consider the potential for liquefaction and lateral spreading on the site to be very low.

We therefore consider future land performance to be in line with Technical Category 1 (TC1), whereby future land damage from liquefaction is unlikely, and ground settlements are expected to be within normally accepted tolerances.

5 RMA Section 106 Requirements and Suitability to Subdivide

Section 106 of the Resource Management Act 1991 states a consent authority may refuse to grant a subdivision consent, or may grant a consent subject to specific consent conditions if it considers that:

- There is a significant risk from natural hazards; or
- Sufficient provision has not been made for legal or physical access to each allotment to be created by the subdivision.

An assessment of the risk from natural hazards as required by the RMA includes the following:

- The likelihood of natural hazards occurring (whether individually or in combination);
- The material damage to land in respect of which the consent is sought, other land, or structures that would result from natural hazards; and
- Any likely subsequent use of the land in respect of which the consent is sought that would accelerate, worsen, or result in material damage of the kind referred to in paragraph (b).

We have assessed the risk of natural hazards at the site in accordance with Section 106 of the Resource Management Act (RMA) and considered the risk to the site from rockfall, inundation (debris), slope stability, subsidence, flooding and tsunami. Based on our observations and the nature of the site, its performance during the CES, and the site's distance from the nearest significant watercourse, we consider it is unlikely for the site to be subject to natural hazards such as rockfall, inundation (debris), slope stability, subsidence, flooding and tsunami. As such, the site is considered suitable for subdivision from a geotechnical perspective.



6 Geotechnical Recommendations

6.1 Earthworks

Earthworks carried out for the subdivision shall be in accordance with NZS 4404:2010, Land Development and Subdivision Infrastructure and NZS 4431:1989, Code of Practice for Earth filling for Residential Development. In particular, any areas to receive fill should be stripped of all vegetation, topsoil, non-engineered fill, soft or organic soils prior to fill placement.

Fill may comprise clean natural sandy gravel or silty soils, or clean imported soils and / or granular fill, compacted to achieve no less than 95% of maximum dry density. Fill faces steeper than 2V:1H and higher than 600 mm should be retained and referred back to ENGEO. Although unlikely, where any springs or groundwater seeps are encountered, they should be intercepted with suitable drainage and discharged to a Council approved outlet.

All unretained batters of pond and stormwater drains constructed with the native sandy gravel material should be at an inclination no steeper than 1V:3H, with protection schemes in place to control erosion of the formed batters within the waterways.

A comprehensive earthworks specification should be provided to the earthworks contractor prior to starting excavations and an inspection / testing regime agreed, along with a robust erosion and sediment control plan.

6.2 Subdivision Roading

Vegetation, any organic or deleterious material, topsoil and non-engineered fill should be removed from the site under pavement areas prior to aggregate placement. Based on our observations during testing, we consider the natural ground below the topsoil at the site should provide an adequate subgrade for the proposed pavement areas.

6.3 Stormwater Control

Concentrated stormwater flows from all impermeable areas must be collected and carried in sealed pipes to the Council system or an alternative disposal point subject to approval from Council. Uncontrolled stormwater must not be allowed to saturate the ground as this will potentially affect future foundation performance both statically and during future seismic activity.

6.4 Foundations

Foundations for future proposed residential dwellings within the subdivision may comprise shallow pad, strip, or slab foundations designed in accordance with the provisions of NZS 3604 Timber Framed Buildings.

Site specific testing will be required for Building Consent, to confirm the bearing materials and capacity. For preliminary design, we anticipate that a geotechnical Ultimate Bearing Capacity of 300 kPa may be assumed for foundations bearing on sandy gravel or engineered fill, below any topsoil. All topsoil shall be stripped from within building footprints, we anticipate this to be typically below 0.3 m depth based on our subsurface investigations.



7 References

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- The Ministry of Business, Innovation, and Employment (2016). New Zealand Geotechnical Database. Retrieved August 2020, from https://www.nzgd.org.nz.



8 Limitations

- i. We have prepared this report in accordance with the brief as provided. This report has been prepared for the use of our client, Hughes Developments Ltd, their professional advisers and the relevant Territorial Authorities in relation to the specified project brief described in this report. No liability is accepted for the use of any part of the report for any other purpose or by any other person or entity.
- ii. The recommendations in this report are based on the ground conditions indicated from published sources, site assessments and subsurface investigations described in this report based on accepted normal methods of site investigations. Only a limited amount of information has been collected to meet the specific financial and technical requirements of the client's brief and this report does not purport to completely describe all the site characteristics and properties. The nature and continuity of the ground between test locations has been inferred using experience and judgement and it should be appreciated that actual conditions could vary from the assumed model.
- iii. Subsurface conditions relevant to construction works should be assessed by contractors who can make their own interpretation of the factual data provided. They should perform any additional tests as necessary for their own purposes.
- iv. This Limitation should be read in conjunction with the Engineering NZ/ACENZ Standard Terms of Engagement.
- v. This report is not to be reproduced either wholly or in part without our prior written permission.

We trust that this information meets your current requirements. Please do not hesitate to contact the undersigned on (03) 328 9012 if you require any further information.

Report prepared by

Jed Watts Engineering Geologist

Report reviewed by

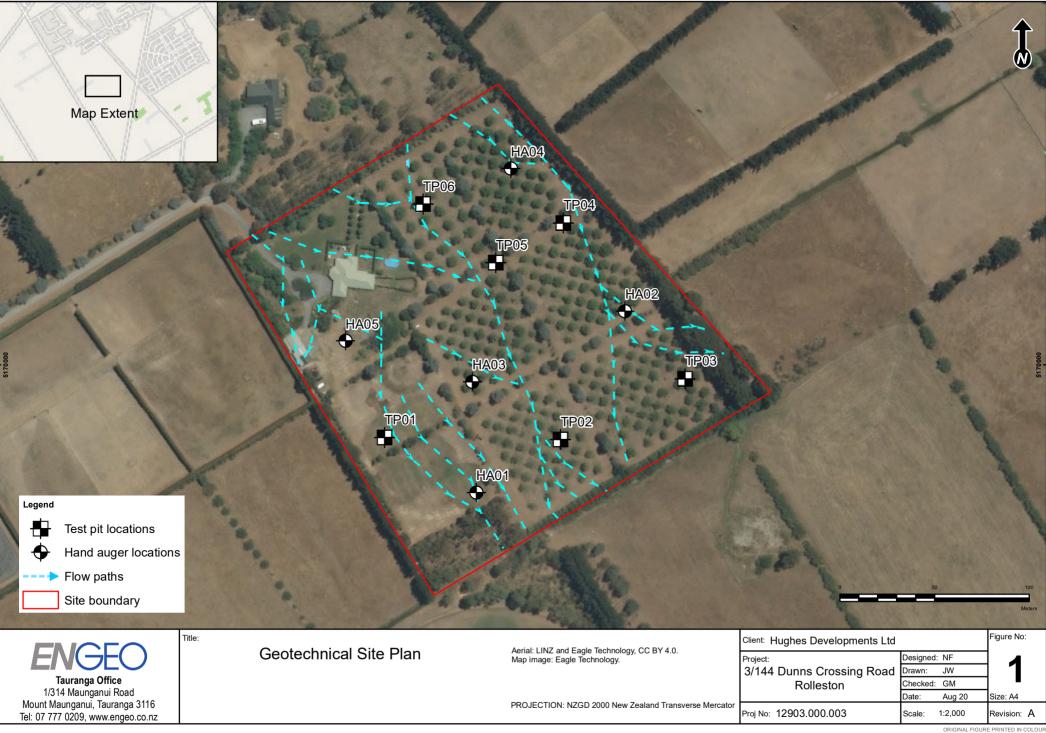
Greg Martin, CMEngNZ (PEngGeol) Principal Engineering Geologist





APPENDIX 1: Site Plan and Inferred Paleo Channels







APPENDIX 2:

ENGEO Hand Auger and Test Pit Logs



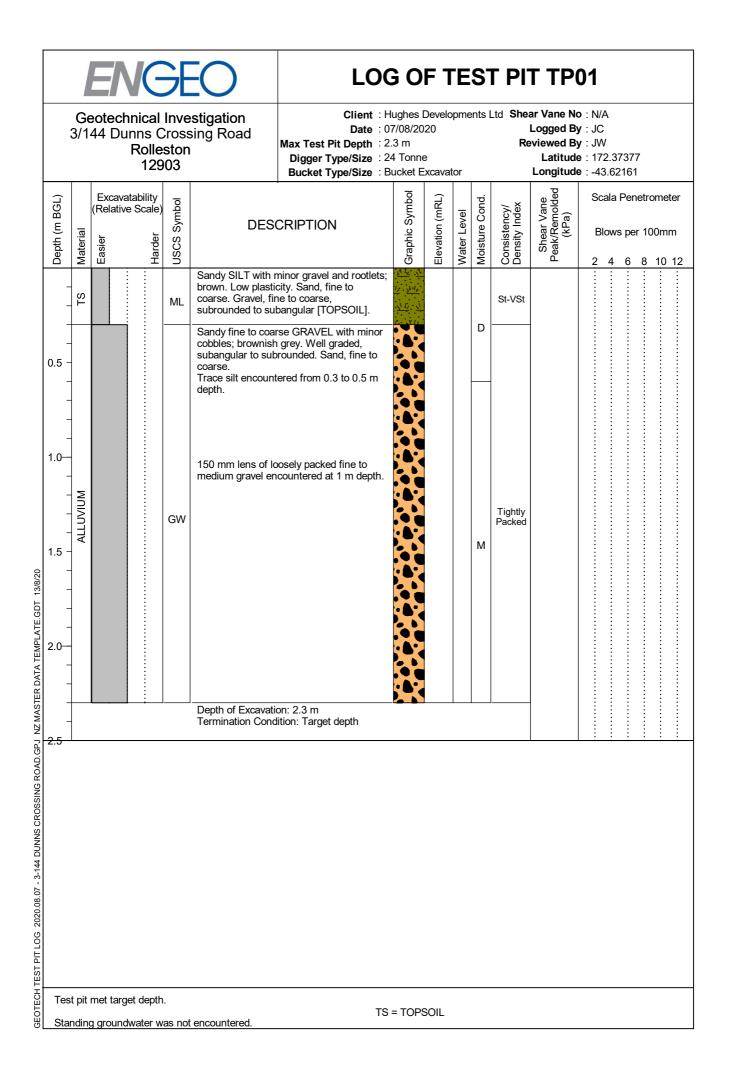
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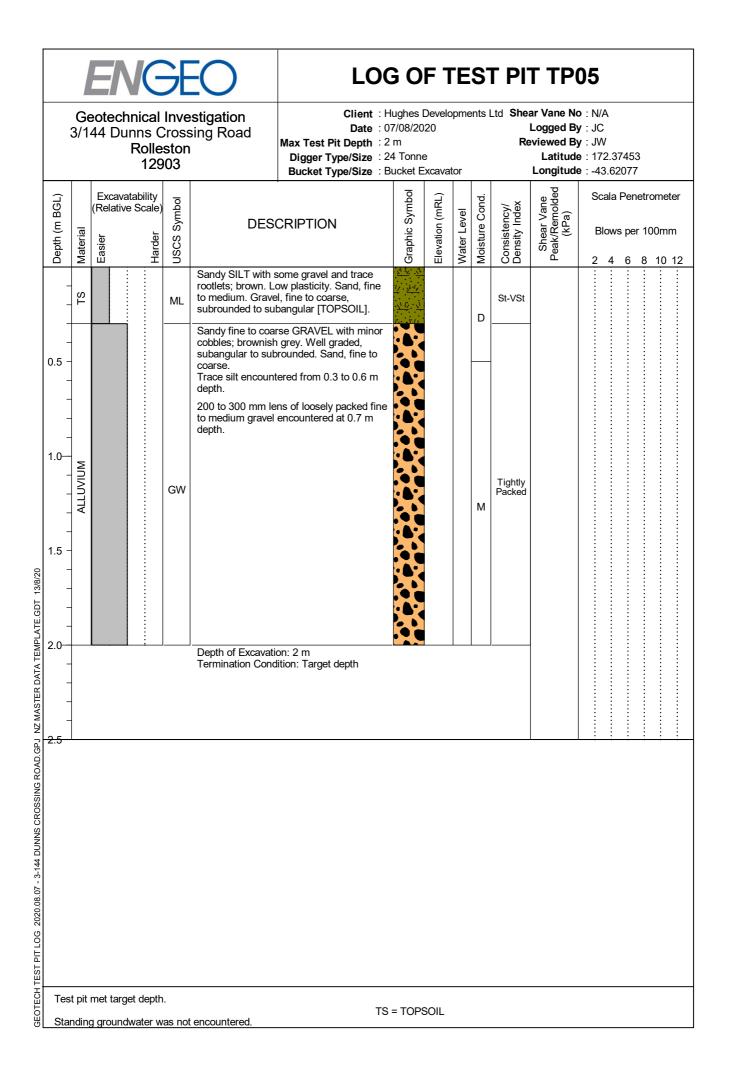
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Bore or Well No	M36/5041		Env	vironment
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Well Number		M36/5041	File Number	CO6C/10302
Owner		KAJENS TRADING DEVELOPMENT LTD	Well Status	Active (exist, present)
Street/Road		DUNNS CROSSING ROAD	NZTM Grid Reference	BX23:49507-69990
Locality		ROLLESTON	NZTM X and Y	1549507 - 5169990
Location Descriptio	'n		Location Accuracy	50 - 300m
CWMS Zone		Selwyn - Waihora	Use	Domestic Supply,
Groundwater Alloca	ation Zone	Selwyn-Waimakariri	Water Level Monitoring	
Depth		32.00m	Water Level Count	0
Diameter		150mm	Initial Water Level	6.80m below MP
Measuring Point De	scription		Highest Water Level	
Measuring Point Ele	evation	40.47m above MSL (Lyttelton 1937)	Lowest Water Level	
Elevation Accuracy	,	< 2.5 m	First reading	
Ground Level		0.00m above MP	Last reading	
Strata Layers		10	Calc Min 80%	9.73m below MP (Estimated)
Aquifer Name			Aquifer Tests	0
Aquifer Type		Unknown	Yield Drawdown Tests	1
Drill Date		01 Feb 1997	Max Tested Yield	5 l/s
Driller		Dynes Road Drilling	Drawdown at Max Tested Yield	13 m
Drilling Method		Cable Tool	Specific Capacity	0.40 l/s/m
Casing Material		STEEL	Last Updated	08 Nov 2013
Pump Type		Unknown	Last Field Check	
Water Use Data		No		

Screens

Screen No.	Screen Type	Top (m)	Bottom (m)	Slot Size (mm)	Slot Length (mm)	Diameter (mm)	Leader Length (mm)
1	Stainless steel	30	32				

Step Tests

Step Test Date	Step	Yield	Yield GPM	DrawDown	Step Duration
01 Feb 1997	1	5.1	67.31074	12.8	2

No comments for this well

Borelog for well M36/5041

Grid Reference (NZTM): 1549508 mE, 5169991 mN Location Accuracy: 50 - 300m Ground Level Altitude: 40.5 m +MSD Accuracy: < 2.5 m Driller: Dynes Road Drilling Drill Method: Cable Tool Borelog Depth: 34.0 m Drill Date: 01-Feb-1997



Scale(m)	Water Level	Depth(m))	Full Drillers Description	Formation Code
			0.0.0.0.0	Small medium gravel very sandy	
Н					
		2.00m	0.0.0.0.0		
Π			0000000000	Small medium gravel siltbound	
Н			000000000		
			000000000		
			000000000		
5		5.40m	000000000		
			0.0.0.0.0	Small medium gravel sand	
			1.0.0.0.0.		
		8.19m	0.0.0.0.0		
			000000000	Small medium gravel siltbound, tight	
			000000000		
10			000000000		
			000000000		
Н			000000000		
Ц			000000000		
		12.80m	000000000		
Н			0000000000	Small medium gravel silt wash gravel brown	
Н			0000000000	brown	
15			000000000		
15			000000000		
-			000000000		
		16.79m	00000000		
			0.0.0.	Small medium gravel sand traces of vellow silt	
-			• • • • • • • • •		
			0.0.0.		
20					
		21.00m			
			0.0.0.0.0	Small medium gravel sandy driving	
Н			0.0.0.00		
Ц			1.0.0.0.0.0.		
			0.0.0.0.0		
Н			0.0.0.0.0		
25		25.40m	***********		
		20.40m	2000000000	Small medium gravel traces silt water	
			000000000	, i i i i i i i i i i i i i i i i i i i	
			000000000		
			000000000		
Ī			000000000		
			0000000000		
30		30.00m			
~~ П		[<u>6.66666666</u>	Small medium gravel gravel small	
Н				almost sand	
Н		32.59m	p.o.o.o.o		
Н			0000000000	Small gravel siltboundwater dropping off	
		34.00m	0000000000	arophing on	

Bore or Well No	M36/0016		En_En	vironment nterbury ional Council ihera Taiao ki Waitaha
Well Name	Goulds Road			nterbury
Owner	WADE.A.		Kaun	ihera Taiao ki Waitaha
Well Number	M36/0016		File Number	
Owner	WADE.A.		Well Status	Not Used
Street/Road	Goulds Road	I	NZTM Grid Reference	BX23:49707-70190
Locality	ROLLESTO	٨	NZTM X and Y	1549707 - 5170190
Location Description			Location Accuracy	50 - 300m
CWMS Zone	Selwyn - Wa	ihora	Use	,
Groundwater Allocation 2	Zone Selwyn-Wair	nakariri	Water Level Monitoring	-
Depth	14.00m		Water Level Count	0
Diameter	51mm		Initial Water Level	
Measuring Point Descript	tion		Highest Water Level	
Measuring Point Elevatio	n 40.62m abov	ve MSL (Lyttelton 1937)	Lowest Water Level	
Elevation Accuracy	< 2.5 m		First reading	
Ground Level	0.00m above	• MP	Last reading	
Strata Layers	3		Calc Min 80%	9.85m below MP (Estimated)
Aquifer Name			Aquifer Tests	0
Aquifer Type	Unknown		Yield Drawdown Tests	0
Drill Date	29 Aug 1932		Max Tested Yield	
Driller	Pearson		Drawdown at Max Tested Yield	
Drilling Method	Unknown		Specific Capacity	
Casing Material	STEEL		Last Updated	06 Mar 2001
Ритр Туре	Unknown		Last Field Check	
Water Use Data	No			

No screen data for this well

No step tests for this well

No comments for this well

Borelog for well M36/0016

Grid Reference (NZTM): 1549708 mE, 5170191 mN Location Accuracy: 50 - 300m Ground Level Altitude: 40.6 m +MSD Accuracy: < 2.5 m Driller: Pearson Drill Method: Unknown Borelog Depth: 15.2 m Drill Date: 29-Aug-1932



Scale(m)	Water Level	Depth(m)		Full Drillers Description	Formation Code
		3.00m .	000000 000000 000000 000000 000000 00000	Stones with clay, hard	
5		9.10m .		Very sandy gravel	
10		15.20m		Small to medium gravel with a little sand	

Bore or Well No	M36/5042		En En	vironment
Well Name	DUNNS CF	ROSSING ROAD		vironment nterbury ional Council hera Taiao ki Waitaha
Owner	KAJENS TI	RADING DEVELOPMENT LTD	Kauni	hera Taiao ki Waitaha
Well Number		M36/5042	File Number	CO6C/10303
Owner		KAJENS TRADING DEVELOPMENT LTD	Well Status	Active (exist, present)
Street/Road		DUNNS CROSSING ROAD	NZTM Grid Reference	BX23:49378-70190
Locality		ROLLESTION	NZTM X and Y	1549378 - 5170190
Location Descriptio	'n		Location Accuracy	50 - 300m
CWMS Zone		Selwyn - Waihora	Use	Domestic Supply,
Groundwater Alloca	ation Zone	Selwyn-Waimakariri	Water Level Monitoring	-
Depth		32.10m	Water Level Count	0
Diameter		150mm	Initial Water Level	6.00m below MP
Measuring Point De	scription		Highest Water Level	
Measuring Point Ele	evation	42.04m above MSL (Lyttelton 1937)	Lowest Water Level	
Elevation Accuracy		< 2.5 m	First reading	
Ground Level		0.00m above MP	Last reading	
Strata Layers		8	Calc Min 80%	9.97m below MP (Estimated)
Aquifer Name			Aquifer Tests	0
Aquifer Type		Unknown	Yield Drawdown Tests	1
Drill Date		01 Nov 1996	Max Tested Yield	5 l/s
Driller		Dynes Road Drilling	Drawdown at Max Tested Yield	12 m
Drilling Method		Cable Tool	Specific Capacity	0.41 l/s/m
Casing Material		STEEL	Last Updated	08 Nov 2013
Pump Type		Unknown	Last Field Check	
Water Use Data		No		

Screens

Screen No.	Screen Type	Top (m)	Bottom (m)	Slot Size (mm)	Slot Length (mm)	Diameter (mm)	Leader Length (mm)
1	Stainless steel	30.1	32.1				

Step Tests

Step Test Date	Step	Yield	Yield GPM	DrawDown	Step Duration
01 Nov 1996	1	5	65.99092	12.2	2

No comments for this well

Borelog for well M36/5042

Grid Reference (NZTM): 1549378 mE, 5170191 mN Location Accuracy: 50 - 300m Ground Level Altitude: 42.0 m +MSD Accuracy: < 2.5 m Driller: Dynes Road Drilling Drill Method: Cable Tool Borelog Depth: 32.5 m Drill Date: 01-Nov-1996



	Water				Formation
Scale(m)	Level	Depth(m)		Full Drillers Description	Code
			000000000000000000000000000000000000000	Small gravel siltbound	
H			000000000000000000000000000000000000000		
H		4.00m	000000000		
5		4.00m		Small medium gravel sandy	
			• • • • • • • • • • • • • • • • • • •		
		8.39m	0.0.0.0.0	Small medium gravel, sandy, wet	
10			0.0.0	yellow silt	
			0:.0:0:		
		12.00m	00.0		
H			000000000000000000000000000000000000000	Small medium gravel siltbound very tight	
Н		14.40m	000000000000000000000000000000000000000		
15			0:. <u>0</u> :0:. .0:.00	Small medium gravel sandy siltenough water to keep sand pump going	
			0:.0:0:		
			0:.0:0		
			00.0.0		
20			00.0.		
Н		22.00-	<u>0:.00</u>		
H		22.00m		Small medium gravel sandy	
		24.20m			
25			000000000000000000000000000000000000000	Small medium gravel brown stain clean	
			20000000000000000000000000000000000000		
		27.60m		Small madium arrival	
				Small medium gravel	
30		m	100000000000 2000000000000 100000000000		
H			00000000000000000000000000000000000000		
Н		32.50m	1000000000000		

Bore or Well No	M36/5038		En En	vironment	
Well Name	DUNNS CROSSING ROAD			nterbury	
Owner	KAJENS TR	ADING DEVELOPMENT LTD	Environment Canterbury Regional Council Kaunihera Taiao ki Waitaha		
Well Number		M36/5038	File Number	CO6C/10010	
Owner		KAJENS TRADING DEVELOPMENT LTD	Well Status	Active (exist, present)	
Street/Road		DUNNS CROSSING ROAD	NZTM Grid Reference	BX23:49278-69840	
Locality		ROLLESTON	NZTM X and Y	1549278 - 5169840	
Location Descriptio	'n		Location Accuracy	50 - 300m	
CWMS Zone		Selwyn - Waihora	Use	Domestic Supply,	
Groundwater Alloca	ation Zone	Selwyn-Waimakariri	Water Level Monitoring	-	
Depth		32.10m	Water Level Count	0	
Diameter		150mm	Initial Water Level	6.30m below MP	
Measuring Point De	scription		Highest Water Level		
Measuring Point Ele	evation	40.38m above MSL (Lyttelton 1937)	Lowest Water Level		
Elevation Accuracy	,	< 2.5 m	First reading		
Ground Level		0.00m above MP	Last reading		
Strata Layers		7	Calc Min 80%	9.58m below MP (Estimated)	
Aquifer Name			Aquifer Tests	0	
Aquifer Type		Unknown	Yield Drawdown Tests	1	
Drill Date		01 Nov 1996	Max Tested Yield	24 l/s	
Driller		Dynes Road Drilling	Drawdown at Max Tested Yield	9 m	
Drilling Method		Cable Tool	Specific Capacity	2.84 l/s/m	
Casing Material		STEEL	Last Updated	08 Nov 2013	
Ритр Туре		Unknown	Last Field Check		
Water Use Data		No			

Screens

Screen No.	Screen Type	Top (m)	Bottom (m)	Slot Size (mm)	Slot Length (mm)	Diameter (mm)	Leader Length (mm)
1	Stainless steel	30.1	32.1				

Step Tests

Step Test Date	Step	Yield	Yield GPM	DrawDown	Step Duration
01 Nov 1996	1	24.1	318.076233	8.5	2

No comments for this well

Borelog for well M36/5038

Grid Reference (NZTM): 1549278 mE, 5169841 mN Location Accuracy: 50 - 300m Ground Level Altitude: 40.4 m +MSD Accuracy: < 2.5 m Driller: Dynes Road Drilling Drill Method: Cable Tool Borelog Depth: 32.0 m Drill Date: 01-Nov-1996



	Water				Formation
Scale(m)	Level	Depth(m)		Full Drillers Description	Code
			0==0==0==	Small gravel silt bound	
Н			==0==0		
Ц			0==0==0==		
			0==0==0		
Н			0.0.0.0.0		
		4.00m	0==0==0		
Π			0.0.0.0.0	small medium gravel sandy	
5					
			1.0.0.0.0.		
-			0.0.0.0.0		
			• ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °		
		8.39m	0.0.0.000		
_			000000000	Small medium gravel with wet yellow silt, small amount of water	
10			000000000000000000000000000000000000000		
10			000000000		
Ц			000000000		
		10.00-	0000000000		
Н		12.00m	0000000000	Small medium gravel siltboundvery	
			000000000	tight	
			000000000		
Н		14.40m			
15			808080808	Small medium gravel, sandyenough	
			0.0.0.0	water to keep hand pump going.	
-			1.0.0.0.0.		
			0.0.0.00		
-			+ 0 · 0 · 0 · 0 · 0 ·		
			0.0.0.0.0		
			p.o.o.o.o.o		
20					
			0.0.0.0		
Н			0.0.0.0.0		
Н		22.00m		<u> </u>	
			0.0.0.0.0.0	Small medium gravel sandy	
H			0.0.0.0.0		
Ц		24.20m			
			0000000000	Small medium gravel brown stain clean	
25			0000000000		
			0000000000		
			000000000000000000000000000000000000000		
			0000000000		
			00000000000		
			0000000000		
-			D0000000000000000000000000000000000000		
30			0000000000		
N		Π	00000000000		
Н			0000000000		
		32.00m			
11		02.0011	a a sa a sa a sa a a a a a a		I