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ENGEO Document Control:

Report Title	Geotechnical Investigation - 182-184 Kepa Road, 8 Kurahaupo Street, Orakei			
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Client Contact Aaron Ghee			Aaron Ghee	
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29/11/2021	REV1 - Update	KW/JC	PF	VB



1 Introduction

ENGEO Ltd was requested by Sanctum Projects Ltd to undertake a geotechnical investigation of the property at 182-184 Kepa Road, 8 Kurahaupo Street, Orakei, Auckland (herein referred to as 'the site').

The purpose of this investigation is to prepare a geological model for the site and outline potential geotechnical constraints to the development as well as to support an application for resource consent for a new five- to eight-storey residential development at the site.

Our scope of work for this investigation is detailed in our proposal dated 16 September 2021 (reference: P2020.002.697 04).

2 Site Description

The site at 182-184 Kepa Road, 8 Kurahaupo Street is located on a total area 2,250 m² and comprises three lots in Orakei, Auckland. The legal descriptions of these lots are Lot 169A DP 50580, SEC 744 Town Orakei, and SEC 745 Town Orakei.

The site currently contains two single-storey dwellings (at 184 Kepa Road and 8 Kurahaupo Street), and a two-storey dwelling at 182 Kepa Road, as well as a standalone garage and sleep-out building at 8 Kurahaupo Street. The site is located in a mixed urban housing area, with residential lots to the north and west of the site. Further west there is a small commercial shopping centre. To the south of the site is Kepa Road (urban route 6), while Kurahaupo Street lies directly to the east.

The majority of the site slopes gently to moderately toward the north at angles of between 5 to 20 degrees, with a fall across the site of approximately 6.5 m from the south-western corner to the northern boundary.

A 150 mm concrete wastewater line passes from east to west through the northern part of the site within 8 Kurahaupo Street. No other service lines are shown on council GIS maps within the site.

3 Proposed Development

ENGEO has been provided with the Monk Mackenzie draft concept architectural plans dated 21October 2021 (unreferenced), which depict the proposed development as consisting of an eight-storey building in the south and a five-storey building in the north, each to be linked by a two-level basement extending across the majority of the site (the ground floor of the eight-storey building will also be below ground along the southern boundary). Due to the slope of the landform, the basement levels day lighted at the northern end of the site.

Based on these plans it is understood that the basement levels will be predominantly utilised for carparking with two residential units in the northern part of the B1 level. The remaining floors will generally consist of residential apartments.

Based on the proposed development plans it is understood that cuts of up to approximately 10.2 m will be required for the basement (including 0.5 m for slab preparation), with maximum cuts expected along the southern site boundary.

The provided concept plans are included in Appendix 1.



4 Desktop Study

4.1 Regional Geology

The site is mapped by GNS Science as being underlain by Auckland Volcanic Field (AVF) basaltic tuff of the Kerikeri Volcanic Group, further underlain by the East Coast Bays Formation material (ECBF) of the Waitemata Group.

Tuff generally consists of an airfall bedded, pulverised mixture of both volcanic and country rock (basaltic sand and scoria, alluvium and Waitemata Group sandstones and siltstones). These range from mud and silt sized particles through to medium to coarse grained sands and occasional gravels and boulders. Material properties reflect considerable variation due to mixed rock types, variable weathering and energy / temperature of emplacement.

East Coast Bays Formation (ECBF) soils are mapped as being located at the ground surface approximately 350 m to the east of the site.

The East Coast Bays Formation was formed in a deep marine setting by turbidity (density) currents during the Miocene Epoch (20 million years ago), resulting in alternating sequences of sandstone and siltstone (termed flysch deposits) which have been measured up to 500 m thick across the wider Auckland region.

In situ weathering of the usually dark grey bedrock material has created, in most locations, an overburden comprising mixtures of silts, clays and sands, being predominantly orange, brown and grey in colour and often containing hard, dark orange-brown iron oxide (limonitic) concentrations which are indicative of long-term fluctuations in groundwater levels. Underlying the East Coast Bays Formation soil there is typically a layer of dark grey, hard, silts and sands, indicative of the transition zone into rock.

4.2 Kepa Road Slip

The Kepa Road Landslide Zone is located on the north-eastern bank of the Orakei Basin. Holocene landslide deposits associated with the Purewa Landslide are mapped approximately 120 m to the south of the site (Figure 1). This material is described as landslide and rockfall detritus, derived from more than one geological unit, and likely contains volcanic, alluvial and ECBF materials.





Figure 1: Kepa Road Landslide Location

Note: Image sourced from Geomaps. Not to scale.

Historical instability has occurred within AVF tuff material overlying ECBF sediments on the steep northeastern side of the Orakei Basin. This is primarily seen within four landslides (Ngapipi Road Landslide, Kepa Road Landslide, St Josephs Landslide, and Pourewa Landslide).

4.3 Seismicity

The Auckland area is one of the lowest earthquake activity regions in New Zealand. Over the last 150 years, only two earthquakes with magnitudes greater than M5 have been recorded in the region.

We have reviewed the GNS New Zealand Active Fault Database, which indicates there are no known active faults on-site. The nearest active fault is the Waikopua Fault located approximately 21 km southeast of the site.

The Kerepehi Fault located in the Hauraki rift zone is considered to pose a significant seismic risk to buildings without specific seismic design across the whole Auckland region.

4.4 Historical Aerial Photography

We have reviewed historic aerial photographs from Auckland Council GIS, Retrolens and Google Earth for years including 1940 to 2017. These photographs were viewed under the context of identifying areas of potential instability and changes to landforms.



- The 1940 photograph showed the site as undeveloped, though Kepa Road and Kurahaupo Street had already been constructed. Neighbouring sites are also undeveloped at this point in time (including the small commercial centre to the west). The scarp of the Kepa Road Landslide to the south of the site was visible in this photo.
- The 1959 photograph showed residential densification in the surrounding area. 182 Kepa Road remains undeveloped. 184 Kepa Road can be seen to be in the early stages of site works, while 8 Kurahaupo is fully developed at this point in time. The commercial centre at 176 Kepa Road has also been constructed.
- The 1968 photograph showed that the dwelling at 184 Kepa Road had been constructed.
- The 1975 photograph showed that the dwelling at 182 Kepa Road had been constructed.
- The site remains generally unchanged from the 1987 photograph.

Aside from the above changes to the site and surrounding area, no obvious signs of changes to landform were observed in the aerial photograph review.

4.5 Existing Geotechnical Information

We have reviewed the New Zealand Geotechnical Database (NZGD) for relevant deep testing data in close proximity to the site.

A machine borehole is located approximately 238 m to the southeast of the site. This borehole encountered AVF and colluvium (silt and clay) to 5 m depth, underlain by extremely weak rock of the ECBF which transitions into very weak rock at 7.7 m depth.

Nine machine boreholes have been uploaded to the NZGD located approximately 430 m southwest of the site on Brenton Place. Material encountered in these boreholes generally consisted of up to approximately 14 m of Auckland Volcanic silts, clays and sands further underlain by very weak to weak Tauranga Group and Waitemata Group weathered soils and rock. Waitemata Group rocks were encountered from between approximately 32.5 mRL to 29.5 mRL within the boreholes.

A singular hand auger that was completed approximately 100 m to the northwest of the site encountered 4 m of Auckland Volcanic field tuff soils.

5 Geotechnical Site Investigation

ENGEO attended site on 20 and 21 October 2021 and completed a geotechnical ground investigation including two machine boreholes (MBH01 and MBH02 in Appendix 2), drilled to 18.05 and 19.65 m below ground level (bgl) respectively. These machine boreholes were drilled using the mud-rotary technique with Standard Penetration Tests (SPT) completed at 1.5 m intervals to assess the *in situ* strength properties of the soil and rock profile. Where possible handheld shear vane measurements were recorded in the end of the core barrel prior to extrusion of the recovered soil.

Standpipe piezometers and continuous groundwater data loggers were installed within both machine boreholes to measure standing groundwater levels beneath the site over a monitoring period that extended from 21 October to 18 November 2021. The standpipe piezometers were slotted between 1.5 and 4.5 m depth and extended from the ground surface to 11.0 m depth, with a bentonite plug at the ground surface and the base of the piezometer.



In addition to the machine boreholes, ENGEO drilled five hand augured boreholes (HA01 through HA05), to 5 meters depth across the site with shear vane readings taken in 30 cm intervals.

Five Scala penetrometer tests (SP01 through SP05) were completed to 1.0 meter depth across the site to gather data to inform California Bearing Ratio assessments for pavement design.

The location of the investigations is presented on the investigation location plan in Appendix 2. Machine borehole and hand auger logs have been prepared in general accordance with the New Zealand Geotechnical Society field classification guidelines (NZGS, 2005) and are presented in Appendix 3, along with borehole core photos. An interpretive ground model based on the findings of the on-site investigation is included in Appendix 4.

5.1 Summary of Subsoil Conditions

Material encountered in the on-site testing generally consisted of the following:

Topsoil was encountered within four of the hand auger boreholes to between 0.1 m and 0.4 m depth.

Near surface fill was encountered in one hand auger borehole to a depth of 0.8 m. The fill was described as intermixed brown and dark brown clay with variable sand content. Fill was also encountered in both of the machine boreholes (which were drilled through paved driveways) to between 0.3 m and 0.8 depth.

Underlying the shallow surface layer of fill and topsoil, native AVF soils comprising layers of clay and silt with variable sand content were encountered across the site to between 54.5 and 49.25 mRL. These soils were typically brown, grey and orange, with measured shear strengths ranging from approximately 50 kPa to in excess of 200 kPa, indicating a stiff to hard soil profile. Average shear strengths were in excess of 140 kPa.

The AVF soils were found to directly overlay up to alluvial silts, clays and sands of the Puketoka Formation which extend to depths of between 51.55 mRL in MBH01 and 46.25 mRL in MBH02. These alluvial soils returned firm to stiff calibrated share vane readings of between 30 and 60 kPa.

Underlying the alluvial soils was ECNF residual soils extending to 48.25 mRL in MBH01 in the southern part of the site and 44.75 mRL in MBH02 in the north.

A thin layer of extremely weak ECBF bedrock was encountered between 44.75 mRL and 44.4 mRL in MBH02.

Very weak ECBF bedrock was encountered from 48.25 mRL in MBH01 in the southern part of the site and from 44.4 mRL in the north. The rock generally comprised of interbedded siltstone and sandstone. The rock was encountered to beyond our maximum testing depth of 19.65 m bgl and was generally found to increase in strength with depth.

5.2 Groundwater Conditions

Groundwater was continuously measured from 21 October to 18 November 2021. During this time groundwater was found to fluctuate between approximately 55.4 mRL (3.6 m depth) and 53.2 mRL (4.8 m depth) in MBH01, and between approximately 53.2 mRL (0.55 m depth) and 51.5 mRL (2.25 m depth) in MBH02 – results of continuous monitoring are included in Appendix 5.



6 Geohazards and Geological Assessment

6.1 Seismic Site Class

For the purposes of seismic design, the site soils have been categorised as Class C, 'Shallow Soil Sites' as described in AS/NZS 1170.5, based on the on-site machine borehole testing.

Based on our understanding of the proposed building, we consider the proposed development to be classified as an Importance Level 2 building. On this basis, we have calculated peak horizontal ground accelerations of 0.19 g and 0.05 g for ULS and SLS conditions, respectively in accordance with MBIE / NZGS Module 1 (2016). The effective earthquake magnitude can be taken as 6.5.

6.2 Seismic Hazard

Soil liquefaction results from loss of strength during cyclic loading, such as imposed by earthquakes. Soils most susceptible to liquefaction are clean, loose, saturated, uniformly graded fine-grained sands. Empirical evidence indicates that loose to medium dense gravels, silty sands, low-plasticity silts, and some low-plasticity clays are also potentially liquefiable.

Based on the material encountered on-site, depth to groundwater and regional setting liquefaction risk at the site is considered to be low.

6.3 Slope Stability

Based on the proposed development plans, it is understood that the majority of slopes at the site will be retained by specifically designed retaining walls. Slope batters formed as part of the development (such as those in the south-eastern part of the site), are expected to be less than 2 m in height and formed to angles of 1V:4H or shallower. If the proposed development concept alters from this, slopes may need to be analysed for stability at the detailed design stage.

7 Groundwater Drawdown

Auckland Council requires an assessment against the Auckland Unitary Plan (AUP): Operative in Part (Table 1), where excavation of materials extends below the groundwater table within the site.

This assessment was based on a proposed basement cut depth of up to approximately 10.2 m which represents the depth below existing ground levels to the finished floor level of level B2 and a 0.5 m allowance for slab thickness and under slab preparations. This equates to a maximum cut depth of approximately 48.4 mRL.

Groundwater levels were measured at levels of between 55.4 mRL and 51.5 mRL (continuously measured within the machine boreholes located in both the north and south of the site).

ENGEO has completed the AUP groundwater assessment for both tanked and drained cases as we have not been advised at this stage whether or not the basement will be drained.

The following tables present an assessment against Standards E7.6.1.6 and E7.6.1.10:



Table 1: E7.6.1.6 Dewatering or Groundwater Level Control Assessment Summary

E7.6.1.6. Dewatering or groundwater level control associated with a groundwater diversion permitted under Standard E7.6.1.10 of the Auckland Unitary Plan

Criteria	Discussion	Assessment Findings	
(1) The water take must not be geothermal water.	Under D1. High-use Aquifer Management Areas Overlay (Auckland Unitary Plan Operative in part) the site is not located in an area marked as a geothermal aquifer.	Criteria Met	
(2) The water take must not be for a period of more than ten days where it occurs in peat soils, or 30 days in other types of soil or rock.	The detailed retaining wall designs have not been completed at this stage. It is likely that the proposed retaining wall design will comprise drained solution and thus will take water for a period greater than 30 days.	Criteria Not Met for Both Cases X	
(3) The water take must only occur during construction.	Groundwater was measured at shallower depths than the proposed basement cuts. It is considered that the basement wall will be drained, therefore we understand that water take will occur following construction.	Criteria Not Met for Drained Case X	



Table 2: E7.6.1.10. Diversion of Groundwater Assessment Summary

E7.6.1.10. Diversion of groundwater caused by any excavation (including trench) or tunnel

Criteria	Discussion	Assessment Findings
 (1) All of the following activities are exempt from the Standards E7.6.1.10 (2) – (6): (a) Pipes cables or tunnels including associated structures which are drilled or thrust and are less than 1.2 m in external diameter. (b) Pipes including associated structures up to 1.5 m in external diameter where a closed faced or earth pressure balanced machine is used. (c) Piles up to 1.5 m in external diameter are exempt from these standards. (d) Diversions for no longer than ten days. (e) Diversions for network utilities and road network linear trenching activities that are progressively opened, closed and stabilised where the part of the trench that is open at any given time is no longer than ten days. 	Not Applicable	Not Applicable
(2) Any excavation that extends below natural groundwater level, must not exceed:a) 1 ha in total area, andb) 6 m depth below the natural ground level.	The proposed cut area is less than 1 ha. However, it is likely to be more than 6 m below ground level in places.	Criteria Not Met for Both Cases
(3) The natural groundwater level must not be reduced by more than 2 m on the boundary of any adjoining site.	The proposed boundary cut level associated with the basement (48.4 mRL) is approximately 3.1 m deeper than the deepest groundwater measurement (51.5 mRL), therefore it is considered that groundwater may be drawn down by more than 2 m on the boundaries of adjoining sites if the walls are drained.	Criteria Not Met for Drained Case X



E7.6.1.10. Diversion of groundwater caused by any excavation (including trench) or tunnel				
 (4) Any structure, excluding sheet piling, that remains in place for more than 30 days, that physically impedes the flow of groundwater through the site must not: (a) Impede the flow of groundwater over a length of more than 20 m. (b) Extend more than 2 m below the natural groundwater level. 	 (a & b) If the proposed basement retaining walls are drained, they are not expected to impede the flow of groundwater. If the walls are tanked they are expected to impede the flow of groundwater over a length of more than 20 m and extend more than 2 m below the natural groundwater level. 	Criteria Not Met for Tanked Case X		
(5) The distance to any existing building or structure (excluding timber fences and small structures on the boundary) on an adjoining site from the edge of any:				
(a) Trench or open excavation that extends below natural groundwater level must be at least equal to the depth of the excavation.	(a) The proposed basement excavation will be closer to neighbouring structures than the depth of the cut (up to 10.2 m deep).	Criteria Not Met for Both Cases		
(b) Tunnel or pipe with an external diameter of 0.2 - 1.5 m that extends below natural groundwater level must be 2 m or greater.	(b) Not applicable.(c) Not applicable.	X		
(c) A tunnel or pipe with an external diameter of up to 0.2 m that extends below natural groundwater level has no separation requirement.				
(6) The distance from the edge of any excavation that extends below natural groundwater level, must not be less than:	(a) No historic wetland management areas from overlay.	Criteria Met		
(a) 50 m from the Wetland Management Areas Overlay.	(b) No historic heritage overlay identified.	\checkmark		
(b) 10 m from a scheduled Historic Heritage Overlay.	(c) Not identified.			
(c) 10 m from a lawful groundwater take.				

As outlined in the tables above, assessment against E7.6.1.6 and E7.6.1.10 of the Auckland Unitary Plan indicates that the proposed development does not meet the criteria to be assessed as a permitted activity.



Resource consent will be required to take and divert groundwater for the proposed development. An assessment of effects report and a draft ground settlement monitoring and contingency plan will be required to support this application.

8 Geotechnical Recommendations

Based on site investigation results, the site is considered to be suitable for the proposed residential development subject to the following recommendations.

8.1 Foundation Recommendations

Due to the likely magnitude of loads generated by the proposed eight-storey building, foundations extending in to or bearing on top of very weak ECBF rock are considered the most appropriate foundation solution for the proposed building.

The proposed basement floor level is set at 48.9 mRL. Very weak sandstone and siltstone bedrock (N≥50) was encountered from approximately 48.25 mRL in MBH01 in the southern part of the site, with very weak rock encountered at 44.4 mRL in MBH02 in the northern part of the site. This rock is considered a suitable bearing stratum for both shallow foundations and bored and concreted piles.

Based on the findings of the geotechnical investigation it is considered that a shallow foundation option may be suitable for the southern extend of the building, while the central and northern parts of the building would likely require a shallow piled foundation bearing on the very weak rock.

An unfactored geotechnical ultimate bearing capacity of 1 MPa is considered to be suitable for shallow foundations bearing on the very weak rock.

For straight-shafted bored and concreted piles drilled into very weak rock, we consider a geotechnical Ultimate End Bearing Capacity of 6 MPa to be suitable at a minimum penetration of four pile diameters.

Geotechnical ultimate side adhesion within the bedrock is assessed to be 450 kPa.

If it is intended to use side friction in conjunction with end bearing capacity, it should be noted that the frictional capacity may fully mobilise before the end bearing capacity and accordingly, it is considered prudent to factor the geotechnical ultimate value by 0.85 prior to applying the appropriate strength reduction factor to allow for the development of residual side adhesion.

If tension piles are required, the contribution of the top metre of bedrock should be ignored in the application of side adhesion.

8.2 Strength Reduction Factor

As required by Section B1/VM4 of the New Zealand Building Code Handbook, a strength reduction factor of 0.50 must be applied to all recommended geotechnical ultimate soil capacities in conjunction with their use in factored design load cases for static and earthquake conditions.



8.3 Basement Excavations

The provided concept plans indicate that the proposed basement encompasses the majority of the site area. Given the close proximity of the basement footprint to existing structures, roads and public services, it is considered that basement retaining will be required along the full southern boundary and the majority of the western and eastern boundaries. This retaining will likely require significant anchoring / propping or be carried out using top-down construction to limit deflections.

At this stage, we have not discussed the preferred wall system with the client and design consultant team. However, an assessment of the Auckland Unitary Plan has been completed in Section 7 of this report. Both drained and tanked basements have their benefits and difficulties and the choice of whether to drain or tank the basement will require consideration of potential effects on neighbouring structures and infrastructure of settlement induced by deflection of the basement retaining wall and settlement caused by groundwater drawdown. A tanked basement will need to include a B2 slab that is double reinforced and thick enough to resist significant uplift pressures within the southern portion of the site.

Groundwater was found to fluctuate between approximately 77.5 mRL (5.1 m depth) and 79 mRL (3.6 m depth) within our monitoring well in the southeast of the site (MBH02).

Considering the proposed basement plans require an excavation of up to 10.2 m depth (including 0.5 m of slab preparation), the excavation depth will likely extend below the groundwater level by several metres. Accordingly, dewatering will be required to facilitate construction of the basement. Consideration should be given to the proximity of the neighboring structures when designing for construction of the basement walls.

A wastewater service line is mapped within the proposed basement excavation area (north). Consideration should be given to the diversion of services to facilitate the excavation of the basement. All services within close proximity of the basement boundary will need to be taken into account during the design of the perimeter retaining wall, and the associated ground settlements that dewatering may cause.

The potential effects of settlements on neighboring structures from groundwater drawdown induced settlements as well as mechanical settlement of the proposed basement retention system will need to be addressed once scheme plans have been finalised. It should involve detailed analysis of a concept wall design to ensure that effects on neighboring structures and infrastructure are less than minor.

8.4 Earthworks Operations

Pre-existing, undocumented fill was encountered to depths between 0.25 m to 0.8 m within the on-site boreholes. At present, ENGEO is not aware of certification or engineering documents detailing the placement and compaction of this fill, and therefore this fill is considered to be non-engineered.

At this stage we have not received earthworks drawings for this development. However, from the plans provided it is anticipated that the earthworks will involve deep cuts of up to approximately 10.2 m below existing ground levels. Given this, it is anticipated that all undocumented fill present on-site will be removed as part of bulk excavations.

Where any fill is required, it should comprise approved clean, hardfill placed in 200 mm lifts and be compacted to a minimum of 95% of maximum dry density, at no less than optimum moisture content.



9 Further Work

As noted in the preceding sections we have yet to receive final development plans and so have not carried out a detailed assessment of effects of the basement excavations on the neighboring properties. Once final levels and layout are confirmed, a concept wall and construction methodology will need to be determined and a concept design of these completed to support an assessment of effects report.

We should then be involved throughout the detailed design process to provide additional geotechnical inputs as required. However, as a minimum we should be given the opportunity to review the final drawings prior to submission for building consent to ensure the assumptions underlying this report are still valid and that our recommendations have been incorporated as intended.

It is also essential that we are given every opportunity to attend a pre-start meeting on site prior to works commencing and then to observe site works, including earthworks operations and ground conditions in foundation and retaining wall excavations (prior to pouring concrete) to confirm works are carried out in accordance with the recommendations of this report and that ground conditions are as assumed.

Upon successful completion of the works we would then be in a position to provide a Producer Statement – Construction Review (PS4).



10 Limitations

- i. We have prepared this report in accordance with the brief as provided. This report has been prepared for the use of our client, Sanctum Projects Ltd, their professional advisers and the relevant Territorial Authorities in relation to the specified project brief described in this report. No liability is accepted for the use of any part of the report for any other purpose or by any other person or entity.
- ii. The recommendations in this report are based on the ground conditions indicated from published sources, site assessments and subsurface investigations described in this report based on accepted normal methods of site investigations. Only a limited amount of information has been collected to meet the specific financial and technical requirements of the client's brief and this report does not purport to completely describe all the site characteristics and properties. The nature and continuity of the ground between test locations has been inferred using experience and judgement and it should be appreciated that actual conditions could vary from the assumed model.
- iii. Subsurface conditions relevant to construction works should be assessed by contractors who can make their own interpretation of the factual data provided. They should perform any additional tests as necessary for their own purposes.
- iv. This Limitation should be read in conjunction with the Engineering NZ / ACENZ Standard Terms of Engagement.
- v. This report is not to be reproduced either wholly or in part without our prior written permission.

We trust that this information meets your current requirements. Please do not hesitate to contact the undersigned on (09) 972 2205 if you require any further information.

Report prepared by

Jacob Cornall

Engineering Geologist

Report reviewed by

Paul Fletcher, CMEngNZ (CPEng)

Associate Geotechnical Engineer

Karl Wright

Engineering Geologist





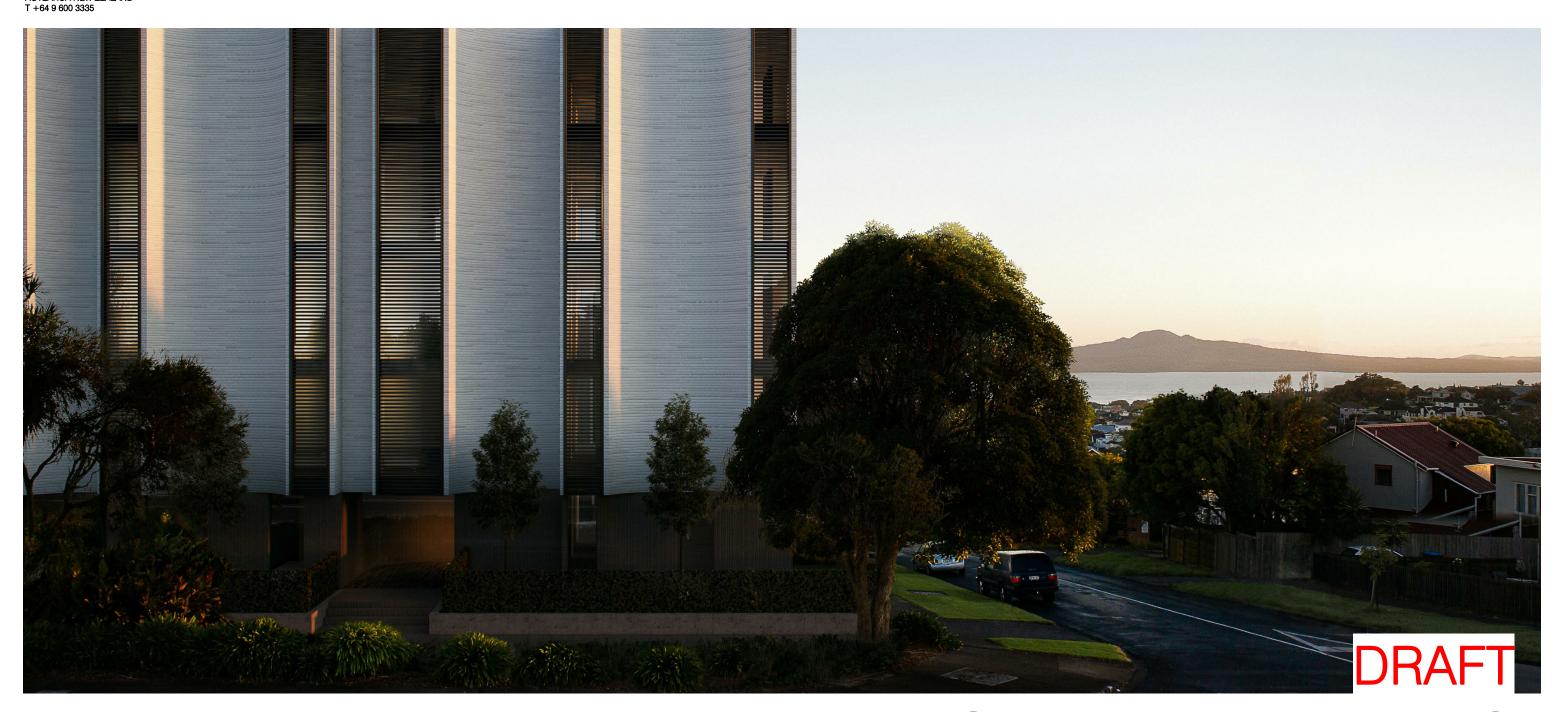
APPENDIX 1:

Proposed Development Plans



MONK MACKENZIE.

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KEPA ROAD APARTMENTS

CONCEPT DESIGN

16.11.21

ARCHITECT CONSULTANT INFORMATION + DOCUMENTATION

MONK MACKENZIE.

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DDO IFOT	INFORMATIO
PHOJECI	INFURMATIO

KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

CLIENT INFORMATION

CLIENT NAME

FILE INFORMATION

FILE LOCATION C:\Users\User\Documents\211020 Kepa Road_Resource Consent_HIRB SET BACK_benny.suen.rvt

DESCRIPTION

DATE STAMP 16/11/2021 2:27:20 PM

ISSUE NOTES

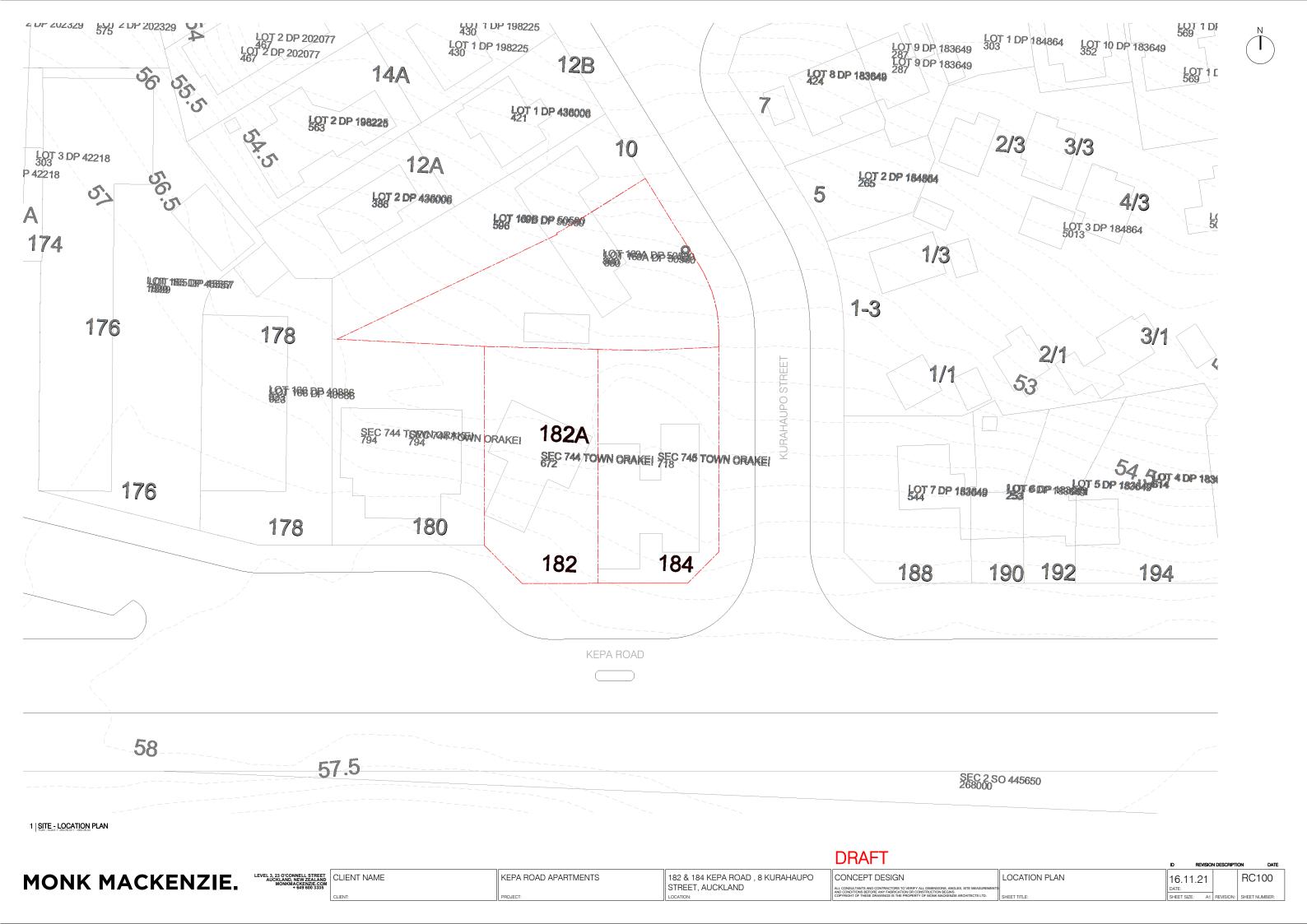
DOCUMENT REVISION INFORMATION

REVISION SCHEDULE

ID DATE

SHEET INDEX SHEET INDEX

SHEET NUMBER	SHEET NAME	CURRENT REVISION
RC000	COVER	
RC001	PROJECT DETAILS	
RC104	SITE METRICS	
RC109	MASTERPLAN - BASEMENT B2	
RC116	MASTERPLAN - L8	
RC118	MASTERPLAN - METRIC	
RC705	PLANNING - HIRB	
RC901	VISUALIZATION - 3D MODEL SHOT	
O.SITE		
RC100	LOCATION PLAN	
RC101	SITE SURVEY	
RC102	SITE DEMOLITION + EXCAVATION PLAN	
RC103	SITE PLAN	
1.PLAN		
RC110	MASTERPLAN - BASEMENT B1	
RC111	MASTERPLAN - L1	
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RC113	MASTERPLAN - L3 & L4	
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RC117	MASTERPLAN - ROOF PLAN	
RC900	VISUALIZATION - 3D MODEL SHOT	
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RC200	ELEVATIONS - NORTH & SOUTH	
RC201	ELEVATIONS - EAST & WEST	
	ELEVATIONS EXOLUTIONS	
3. SECTIONS	CECTIONIC MORTH COLITH CECTION	
RC300 RC301	SECTIONS - NORTH SOUTH SECTION SECTIONS - WEST EAST SECTION	
NC301	(BLOCK A)	
RC302	SECTIONS - WEST EAST SECTION (BLOCK B)	
7.PLANNING		
RC700	PLANNING - OUTDOOR LIVING	
RC701	PLANNING - OUTDOOR LIVING	
RC702	PLANNING - OUTLOOK	
RC703	PLANNING - OUTLOOK	
RC710	SHADOW STUDIES - EQUINOX (23 SEP & 20 MARCH)	
RC711	SHADOW STUDIES - SUMMER	
0.0743	SOLSTICE (22 DEC)	
RC712	SHADOW STUDIES - WINTER SOLSTICE (21 JUN)	





NOTE: PLEASE REFER TO THE TOPOGRAPHIC SURVEY DONE BY CIVIX.

1 | SITE - SURVEY PLAN

DRAFT

MONK MACKENZIE.

LEVEL 3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND MONKMACKENZIE COM H 649 600 3335

IENT NAME KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND LOCATION: CONCEPT DESIGN

ALL CONSULTANTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, SITE MEASUREMENTS AND CONDITIONS BEFORE ANY FABRICATION OR CONSTRUCTION BEGINS.

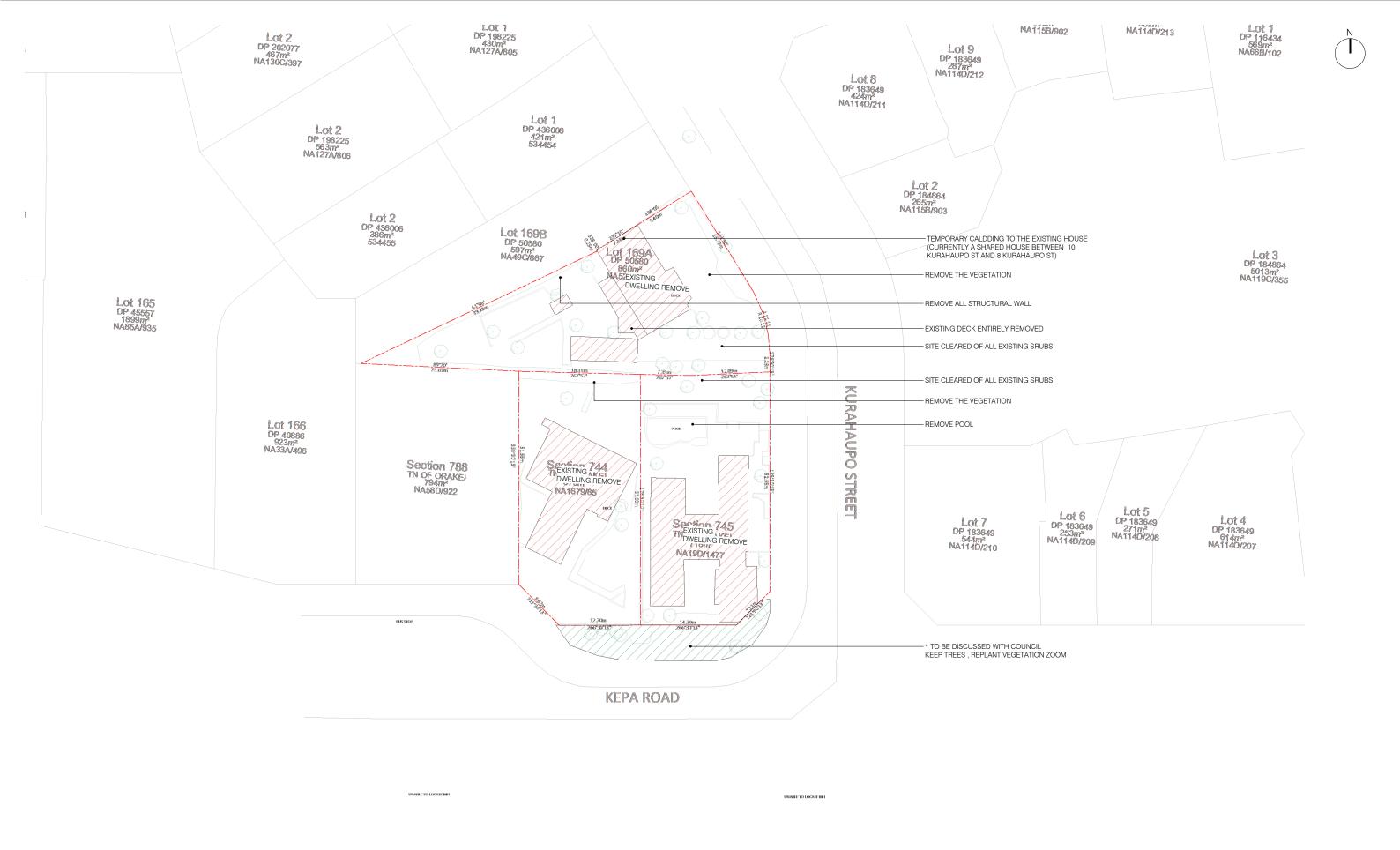
SHEET TITLE:

SHEET TITLE:

SITE SURVEY

16.11.21 RC101

DATE:
SHEET TITLE:
SHEET SIZE: A1 REVISION: SHEET NUMBER



1 | SITE - DEMOLITION EXCAVATION PLAN

DRAFT

MONK MACKENZIE.

LEVEL 3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND MONKMACKEVIZE COM MONKMACKEVIZE COM + 649 600 3335

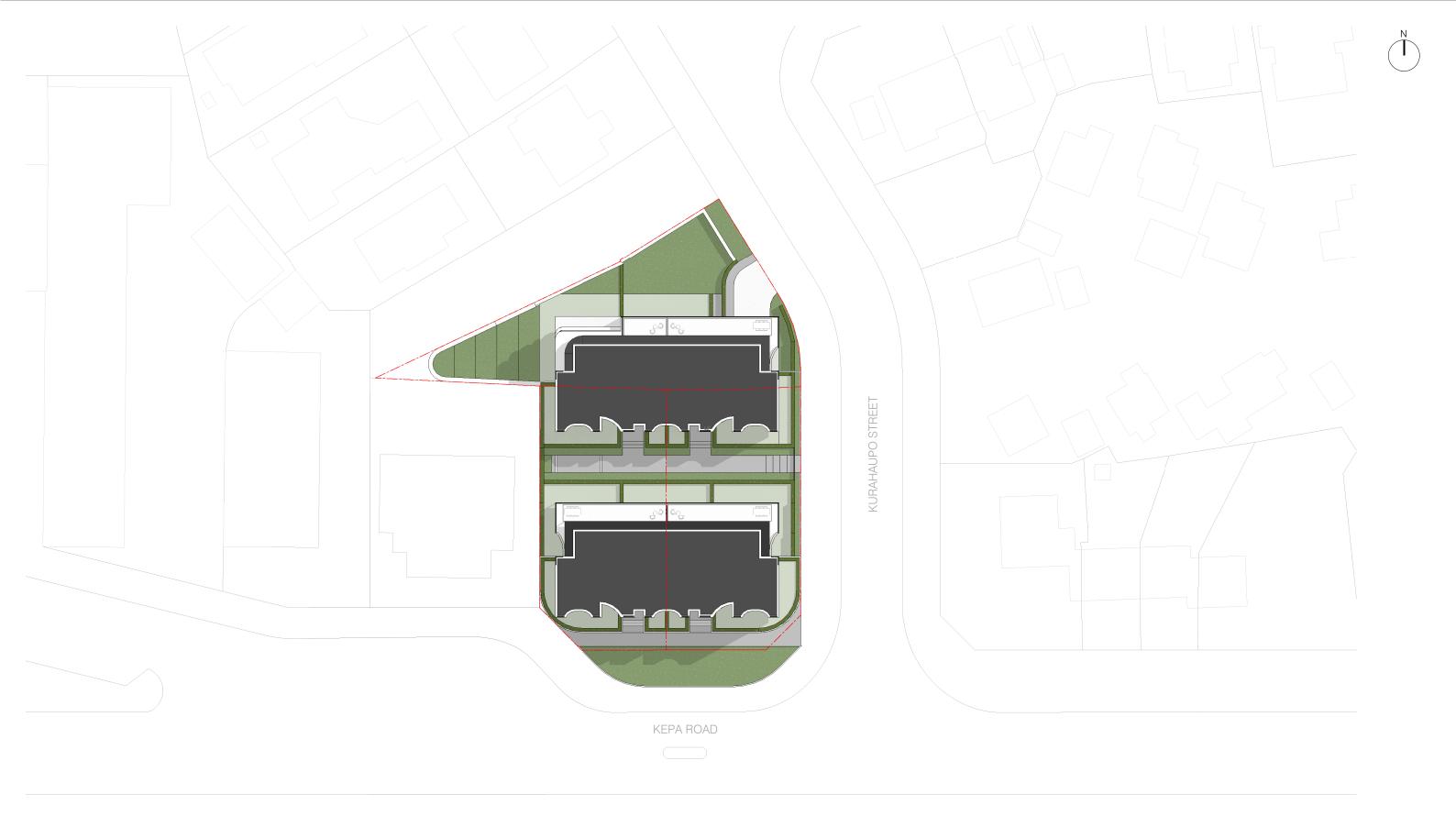
AME KEPA ROAD APARTMENTS

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AND CONDITIONS BEFORE ANY FABRICATION OR CONSTRUCTION BEGINS.
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SITE DEMOLITION + EXCAVATION PLAN

16.11.21 RC102
DATE:
SHEET SIZE: A1 REVISION: SHEET NUMBER:



1 | SITE - SITE PLAN

DRAFT

MONK MACKENZIE.

LEVEL 3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND MONKMACKENZIE COM MONKMACKENZIE COM 1649 600 3335

CLIENT NAME

CLIENT NAME

A 449 600 3335

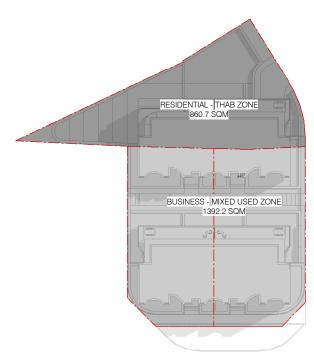
KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

CONCEPT DESIGN

SITE PLAN

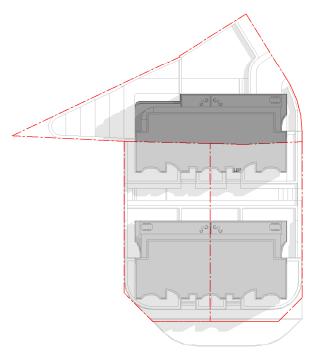
16.11.21 RC103



1 | METRIC - SITE AREA

RESIDENTIAL - THAB ZONE AREA | 860.7 SQM

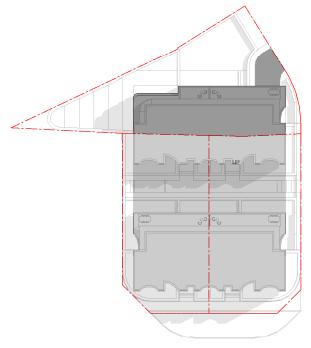
BUSINESS - MIXED USED ZONE AREA | 1392.2 SQM



2 | METRIC - BUILDING COVERAGE

RESIDENTIAL - THAB ZONE BUILDING COVERAGE AREA $\,\mid$ 317.9 SQM THAB ZONE AREA $\,\mid$ 36.9% (MAX 50% \mid COMPLY)

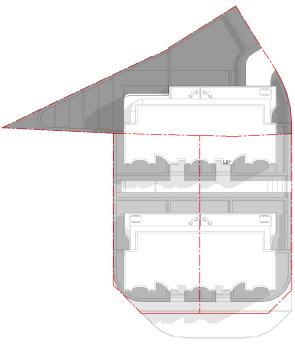
BUSINESS - MIXED USED ZONE BUILDING COVERAGE AREA $\,|\,$ 694.7 SQM MIXED USED ZONE $\,\%\,\,|\,$ 49.9% (N/A)



3 | METRIC - IMPERVIOUS AREA

RESIDENTIAL - THAB ZONE IMPERVIOUS AREA | 355.3QM THAB ZONE AREA %| 41.3% (MAX 70% | COMPLY)

BUSINESS - MIXED USED ZONE IMPERVIOUS AREA $\,|\,$ 1040.9 SQM MIXED USED ZONE % $|\,$ 74.7% (N/A)



4 | METRIC - LANDSCAPE AREA

RESIDENTIAL - THAB ZONE LANDSCAPE AREA | 505.4 SQM THAB ZONE AREA %| 58.7% (MIN 30% | COMPLY)

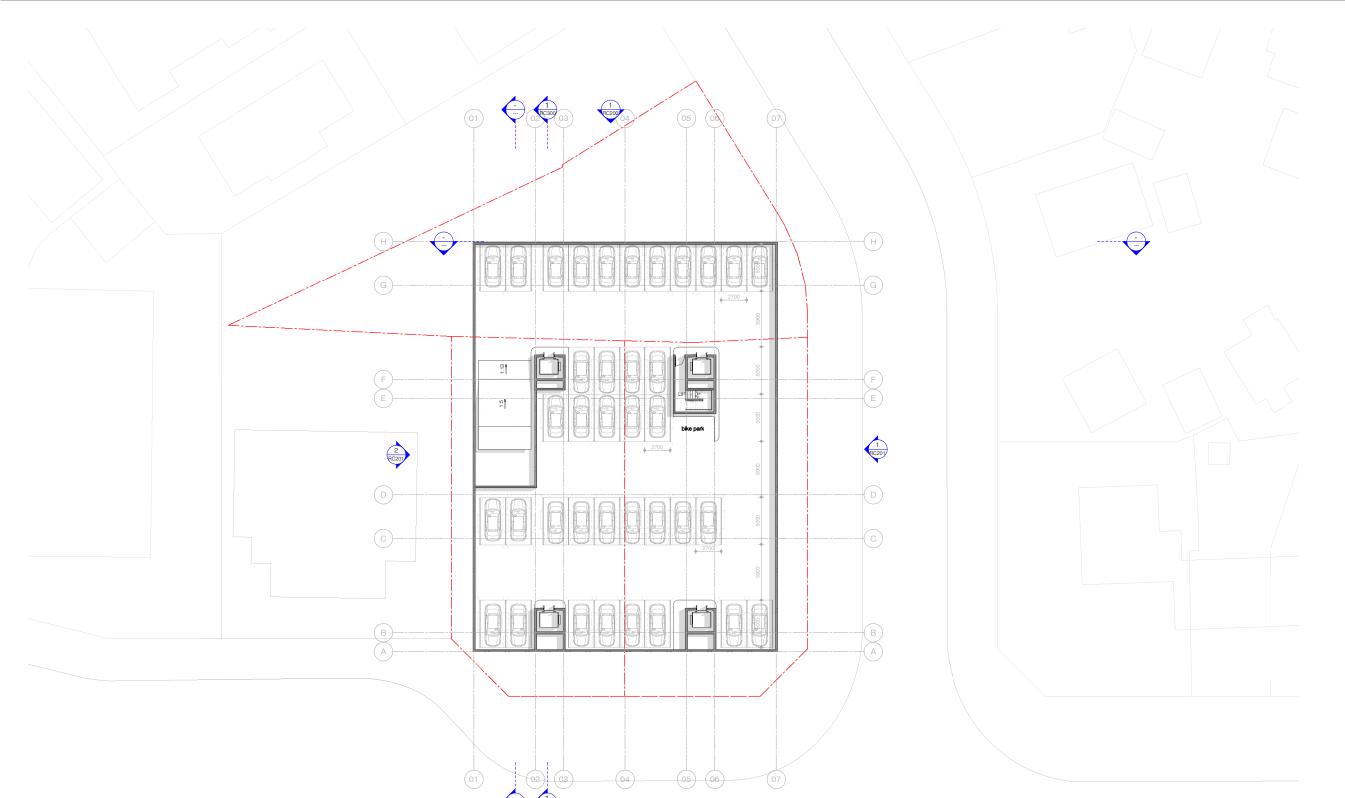
BUSINESS - MIXED USED ZONE LANDSCAPE AREA $\,|\,$ 489.9 SQM MIXED USED ZONE % $\,|\,$ 35.2% (N/A)

KEPA ROAD APARTMENTS

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RC104 16.11.21



AREA SCHEDULE (GFA) _ BASEMENT B2

1 BASEMENT B2

DRAFT

MONK MACKENZIE.

LEVEL 3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND MONKMACKENZIE, COM MONKMACKENZIE, COM 40 600 3335

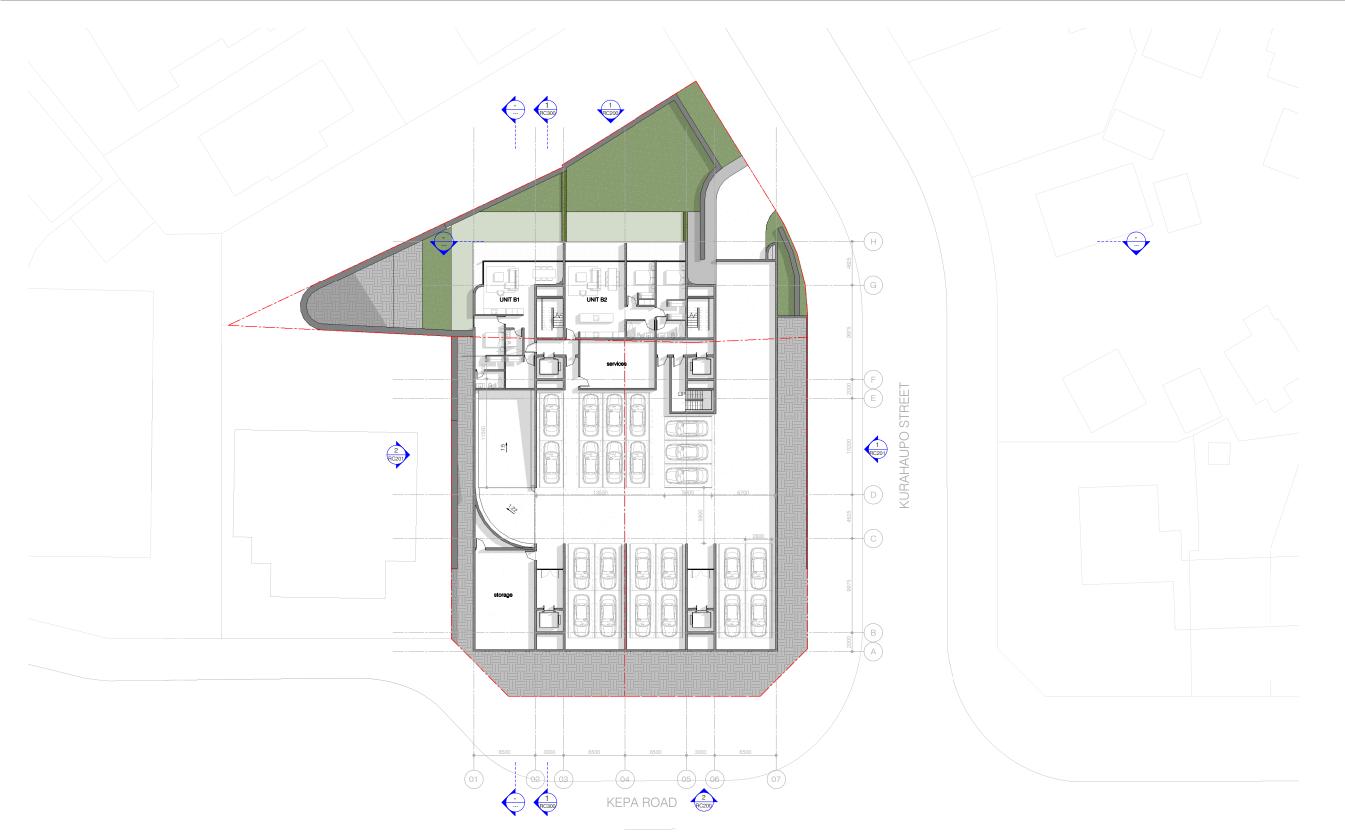
KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

CONCEPT DESIGN

MASTERPLAN - BASEMENT B2

16.11.21



AREA SCHEDULE (GFA) _ BASEMENT B1

CARPARK	854.52	
CIRC.		
CIRCULATION	26.06 n	
CIRCULATION	26.06 n	
CIRCULATION	35.80 n	
CIRCUILATION	57 23 n	

DRAFT

1 BASEMENT B1

KEPA ROAD APARTMENTS

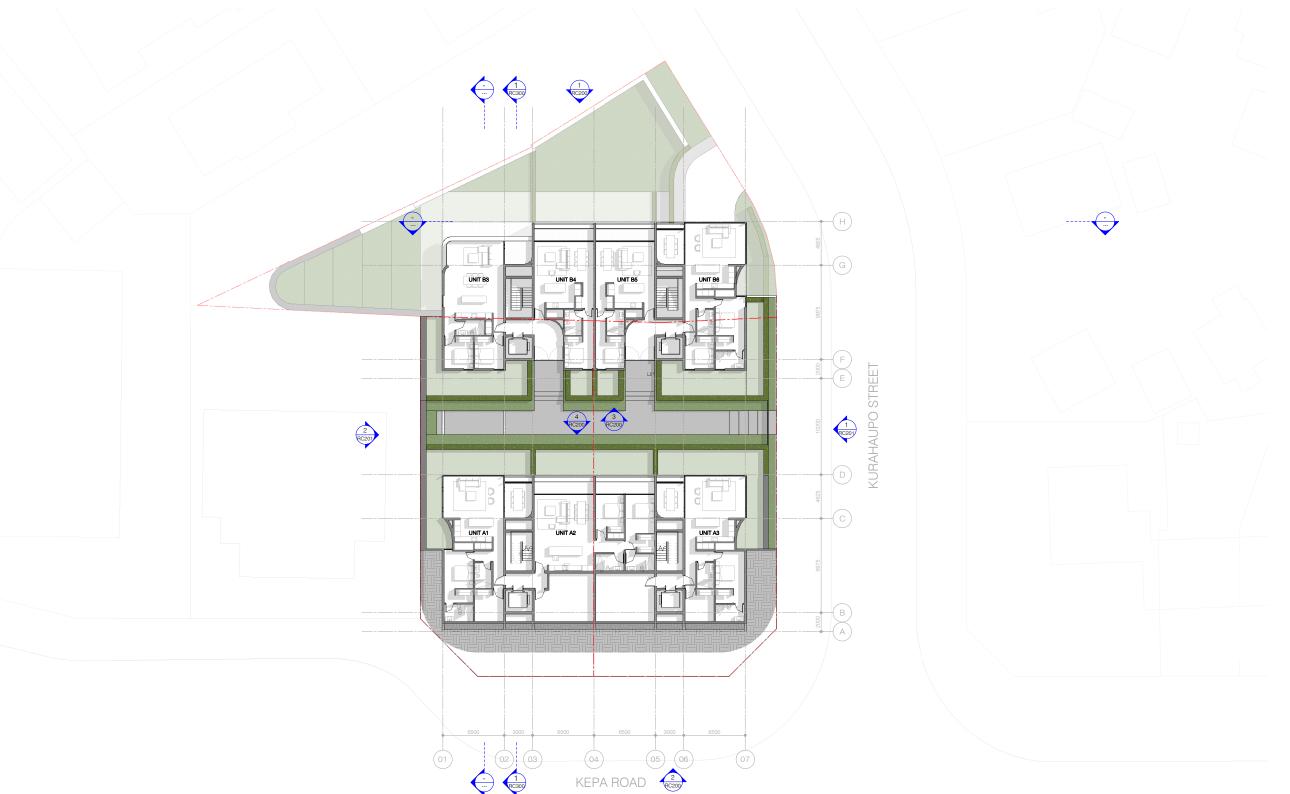
182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

CONCEPT DESIGN

MASTERPLAN - BASEMENT B1

16.11.21

RC110



UNIT B5

APARTMENT 7
PATIO
GARDEN

UNIT B6

APARTMENT 101.19 |

GARDEN 58.05 |

PATIO 11.80 |

MONK MACKENZIE.

1 | LEVEL 1 PLAN - SCALE 1: 200 ON A#1: 200 ON A3



DRAFT

MONK MACKENZIE.

1 | LEVEL 2 PLAN - SCALE 1: 200 ON A/11: 200 ON A3

LEVEL 3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND MONKMACKENZIE. COM MONKMACKENZIE. COM MONKMACKENZIE. COM MONKMACKENZIE. COM

KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

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MASTERPLAN - L2

RC112 16.11.21





UNIT ID	Area
I FO IFFE	
LEVEL 4	
CIRC.	
CIRCULATION	32.17
UNIT A12	
APARTMENT	104.52
PATIO	11.80
UNIT A13	
APARTMENT	93.17
PATIO	8.00
UNIT A14	
APARTMENT	93.17
PATIO	8.00
UNIT A15	
APARTMENT	104.49
PATIO	11.80
UNIT B15	
APARTMENT	78.48
PATIO	22.69
LINET DAY	
UNIT B16 APARTMENT	93.17
PATIO	8.00
FAIIO	0.00
UNIT B17	
APARTMENT	93.17
PATIO	8.00
UNIT B18	
	104.49
APARTMENT	104.49

1 | LEVEL 3 & LEVEL 4

DRAFT

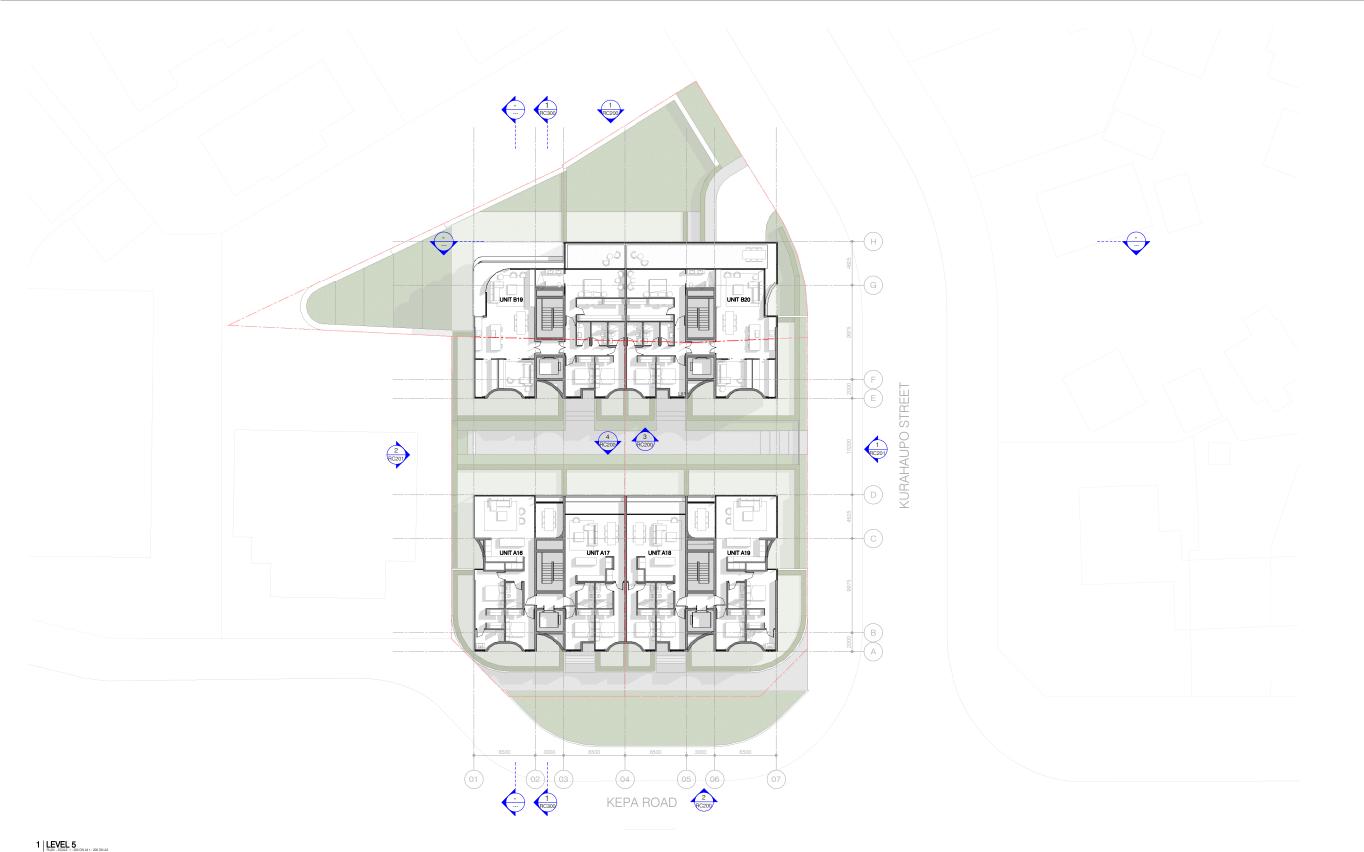
LEVEL 3, 23 O'CONNELL STREET
AUGKLAND, NEW ZEALAND
MONKMACKENZIE COM
+ 649 600 3335

CLIENT NAME

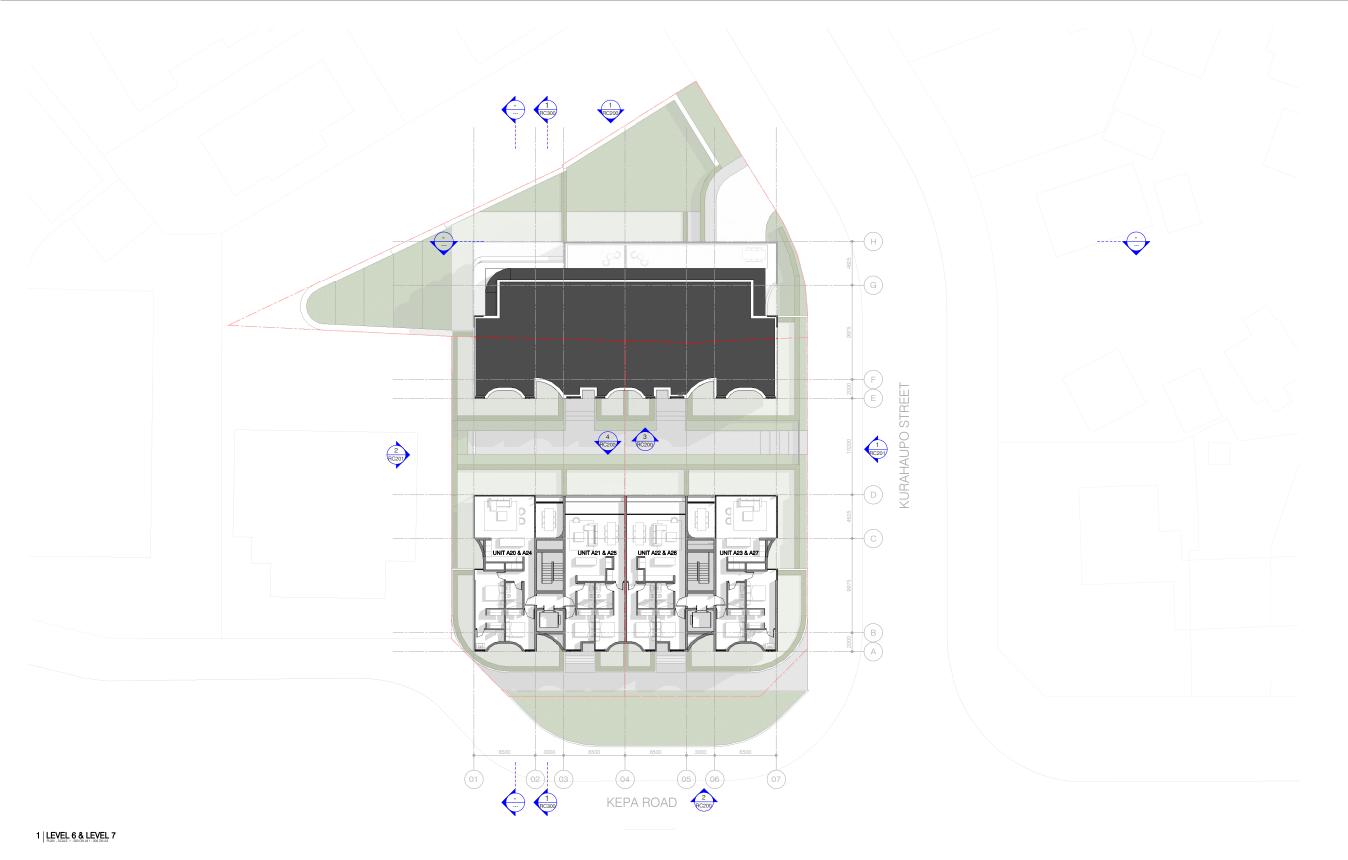
KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO
STREET, AUCKLAND

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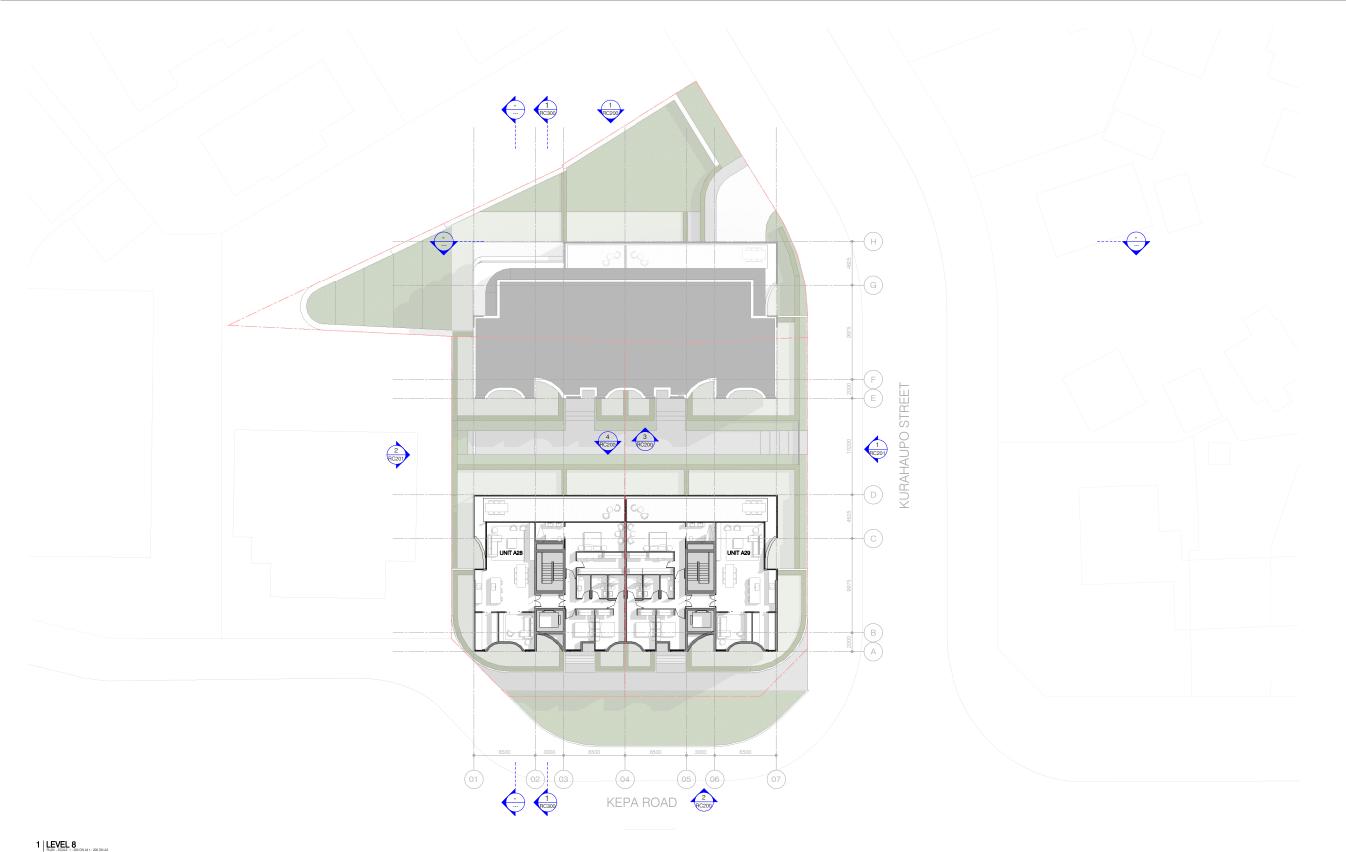






UNIT ID	Area
LEVEL 6	
CIRC.	
CIRCULATION	32.17
CIRCULATION	32.17
UNIT A20	
APARTMENT	104.52
PATIO	11.80
UNIT A21	
APARTMENT	93.17
PATIO	8.00
UNIT A22	
APARTMENT	93.17
PATIO	8.00
UNIT A23	
APARTMENT	104.49
PATIO	11.80

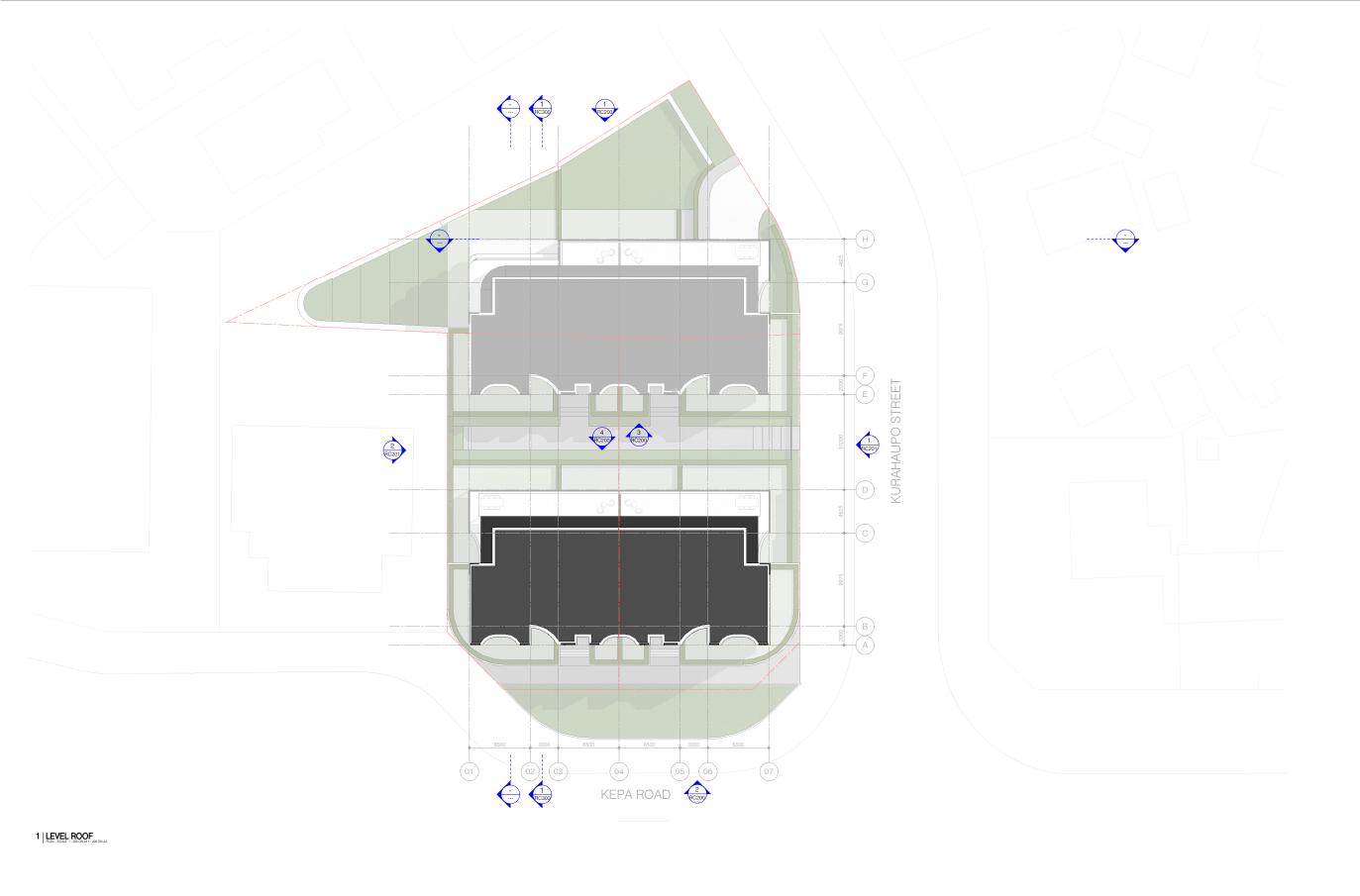
UNIT ID	Area
LEVEL 7	
CIRC.	
CIRCULATION	3
CIRCULATION	3
UNIT A24	
APARTMENT	10
PATIO	1
UNIT A25	
APARTMENT	g
PATIO	
UNIT A26	
APARTMENT	9
PATIO	



CIRC.		
CIRCULATION	30.97	
CIRCULATION	30.97	

UNIT A28	
APARTMENT	176.53 m ²
PATIO	48.49 m ²

176.48 m² 48.50 m²



DRAFT

LEVEL 3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND NEW



9 | LEVEL 7

8 | LEVEL 4 PLAN - SCALE 1 : 500 ON A/1 : 1000 ON AS

2 | LEVEL 1 | PLAN - SCALE 1 : 500 CIN A/1 : 1000 CIN A3

	JLE (GFA)	AREA SCHED	
UNIT ID	Area	UNIT ID	Area
ASEMENT B2 ASEMENT		UNIT B9 APARTMENT	93.17 m²
ARPARK	1244.25 m²	PATIO	93.17 m² 8.00 m²
IRC.		UNIT B10	
RCULATION	10.50 m ²	APARTMENT	104.43 m²
IRCULATION IRCULATION	25.95 m ² 13.50 m ²	PATIO	11.80 m²
IRCULATION	13.50 m²	LEVEL 3	
ASEMENT B1		CIRC. CIRCULATION	32.17 m ²
ASEMENT		CIRCULATION	32.17 m ²
ARPARK	854.52 m ²	CIRCULATION CIRCULATION	32.17 m ² 32.17 m ²
IRC.			02.17 ITE
CIRCULATION CIRCULATION	26.06 m ² 26.06 m ²	UNIT A8 APARTMENT	104.52 m²
CIRCULATION	35.80 m²	PATIO	104.52 m² 11.80 m²
CIRCULATION	57.23 m ²	UNIT A9	
ERVICE		APARTMENT	93.17 m ²
ERVICE ERVICE	82.11 m ² 43.17 m ²	PATIO	8.00 m ²
	40.17 HP	UNIT A10	
NIT B1 PARTMENT	95.78 m²	APARTMENT PATIO	93.17 m ² 8.00 m ²
ARDEN	214.10 m ²		0.00111
ATIO	21.45 m ²	UNIT A11 APARTMENT	104.49 m²
NIT B2		PATIO	11.80 m ²
PARTMENT ATIO	109.87 m ² 12.25 m ²	UNIT B11	
ATIO	12.25 m ²	APARTMENT	94.04 m ²
ARDEN	195.53 m²	PATIO	8.42 m ²
EVEL 1		UNIT B12	
CIRC. CIRCULATION	44.68 m²	APARTMENT PATIO	93.17 m ² 8.00 m ²
IRCULATION	44.59 m²		0.001111
IRCULATION IRCULATION	36.35 m ² 33.47 m ²	UNIT B13 APARTMENT	93.17 m ²
•	55.47 HF	PATIO	8.00 m ²
ERVICE ERVICE	67.64 m²	UNIT B14	
•	07.34111	APARTMENT	104.49 m²
NIT A1 PARTMENT	101.09 m²	PATIO	11.80 m ²
ARDEN	59.53 m²	LEVEL 4	
ATIO	11.80 m²	CIRC. CIRCULATION	32.17 m²
JNIT A2		CIRCULATION	32.17 m ²
PARTMENT	109.40 m ²	CIRCULATION	32.17 m ²
ATIO ATIO	8.00 m ²	CIRCULATION	32.17 m ²
ARDEN	41.60 m²	UNIT A12	
NIT A3		APARTMENT PATIO	104.52 m ² 11.80 m ²
PARTMENT	101.09 m²		
ARDEN ATIO	59.36 m ² 11.80 m ²	UNIT A13 APARTMENT	93.17 m²
•		PATIO	8.00 m ²
INIT B3 PARTMENT	90.72 m²	UNIT A14	
GARDEN	53.49 m²	APARTMENT	93.17 m²
ATIO	8.42 m ²	PATIO	8.00 m ²
INIT B4	70.//	UNIT A15	40
PARTMENT ATIO	72.41 m ² 8.00 m ²	APARTMENT PATIO	104.49 m ² 11.80 m ²
ARDEN	9.76 m ²		**************************************
NIT B5		UNIT B15 APARTMENT	78.48 m²
PARTMENT	72.49 m²	PATIO	22.69 m²
ATIO ARDEN	8.00 m ² 9.78 m ²	UNIT B16	
		APARTMENT	93.17 m²
NIT B6 PARTMENT	101.19 m²	PATIO	8.00 m ²
ARDEN	58.05 m ²	UNIT B17	
ATIO	11.80 m²	APARTMENT PATIO	93.17 m ² 8.00 m ²
EVEL 2			0.00111
CIRC.	44.68 m ²	UNIT B18 APARTMENT	104.49 m²
IRCULATION	44.59 m²	PATIO	104.49 m² 11.80 m²
IRCULATION IRCULATION	32.17 m ² 32.17 m ²	LEVEL 5	
•	06.17 IIIs	CIRC.	
INIT A4	101.01	CIRCULATION	32.17 m ²
PARTMENT BARDEN	101.21 m ² 46.35 m ²	CIRCULATION	32.17 m ² 30.97 m ²
PATIO	11.80 m ²	CIRCULATION	30.97 m ²
NIT A5		UNIT A16	
PARTMENT	72.41 m²	APARTMENT	104.52 m²
ATIO	8.00 m ²	PATIO	11.80 m²
ARDEN	9.29 m²	UNIT A17	
	70.00	APARTMENT	93.17 m²
	72.49 m² 8.00 m²	PATIO	8.00 m ²
PARTMENT		UNIT A18	
JNIT A6 PARTMENT PATIO GARDEN	9.29 m²		
PARTMENT PATIO GARDEN		APARTMENT	93.17 m²
PARTMENT PATIO GARDEN JNIT A7 PARTMENT			93.17 m ² 8.00 m ²
PARTMENT ATIO ARDEN NIT A7 PARTMENT ARDEN	9.29 m ² 101.19 m ² 55.80 m ²	APARTMENT PATIO UNIT A19	8.00 m²
PARTMENT ATIO SARDEN INIT A7	9.29 m² 101.19 m²	APARTMENT PATIO UNIT A19 APARTMENT	8.00 m ² 104.49 m ²
PARTMENT ATIO ARDEN NIT A7 PARTMENT ARDEN	9.29 m ² 101.19 m ² 55.80 m ²	APARTMENT PATIO UNIT A19	8.00 m²

AREA SCHEDULE (GFA)

DRAFT

MONK MACKENZIE.

LEVEL3, 23 O'CONNELL STREET AUCKLAND, NEW ZEALAND MONKMACKENZIE, COM + 649 600 3335

CLIENT NAME

KEPA ROAD APARTMENTS

KEPA ROAD APARTMENTS

STREET, AUCKLAND

AL CONSULTANTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO VERY ALL DIMENSIONS, ANGLES, STRE MEASUREMENTS AND CONTRACTORS TO V



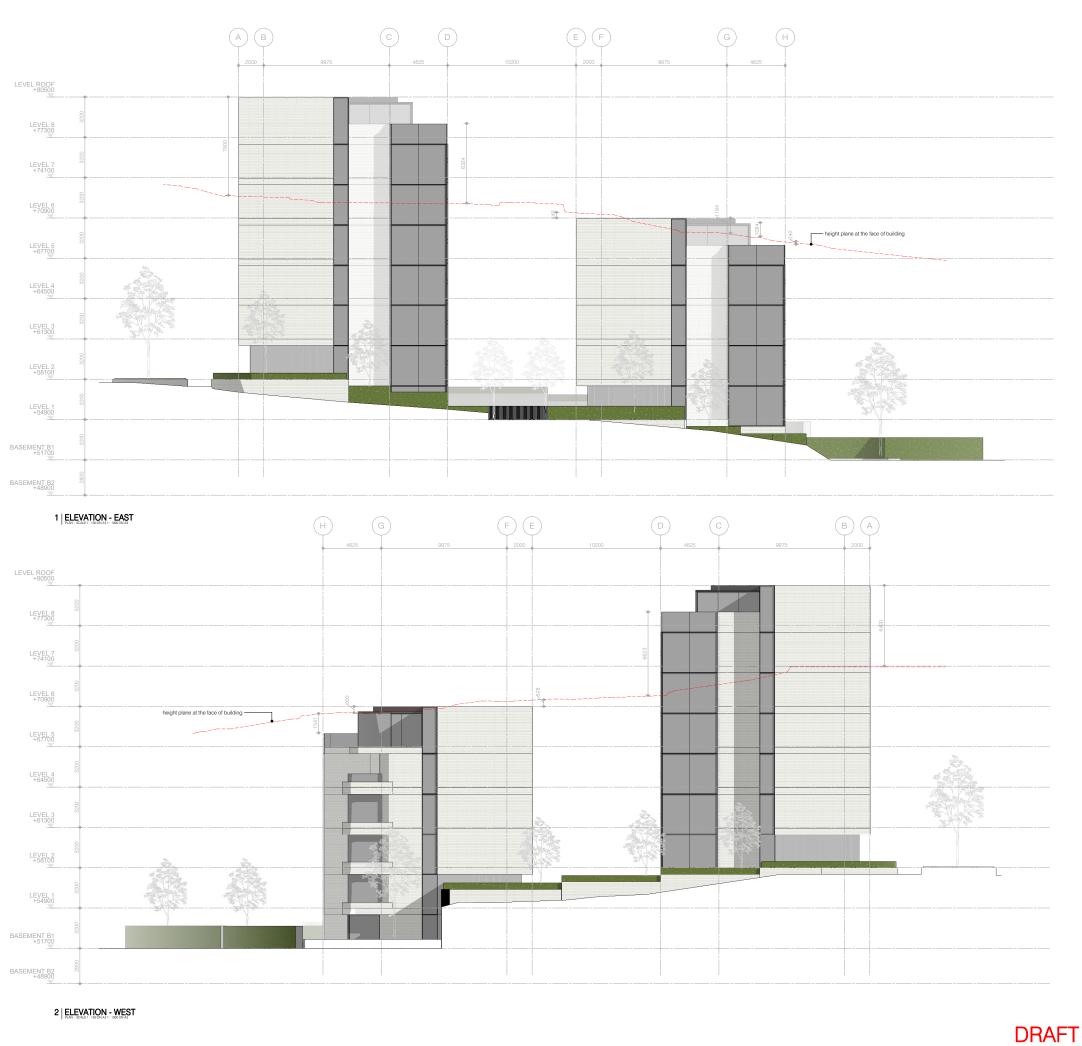
MONK MACKENZIE.

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ELEVATIONS - NORTH & SOUTH

RC200 16.11.21



MONK MACKENZIE.

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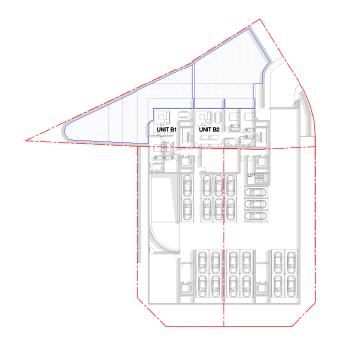
KEPA ROAD APARTMENTS

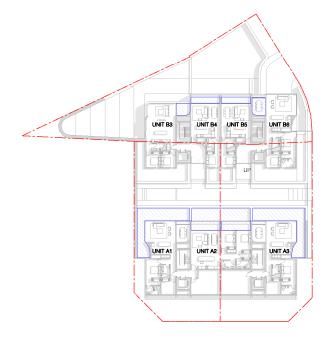
182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

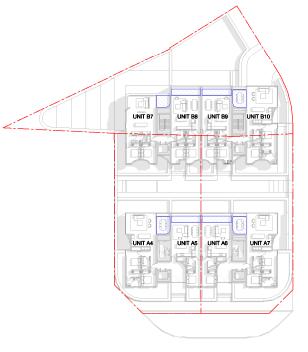
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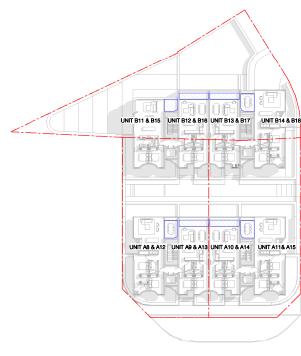
ELEVATIONS - EAST & WEST

16.11.21 RC201









1 OUTDOOR - BASEMENT

DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT BASEMENT LEVEL

UNIT B1 | 202.7 SQM

UNIT B2 | 188.6 SQM

2 OUTDOOR - LEVEL 1

DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT LEVEL 1

UNIT A1 | 45.7 SQM UNIT A2 | 58.3 SQM UNIT A3 | 45.7 SQM UNIT B3 | 7.1 SQM

UNIT B4 | 8 SQM UNIT B5 | 8 SQM UNIT B6 | 10.4 SQM

4 OUTDOOR - LEVEL 2

UNIT A4 | 10.4 SQM

DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT LEVEL 2

UNIT A5 | 8 SQM UNIT A6 | 8 SQM UNIT A7 | 10.4 SQM UNIT B7 | 7.1 SQM UNIT B8 | 8 SQM UNIT B9 | 8 SQM UNIT B10 | 10.4 SQM

3 OUTDOOR - LEVEL 3 & LEVEL 4

DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT LEVEL 3 & 4

UNIT A8 & A12 | 10.4 SQM UNIT A9 & A13 | 8 SQM UNIT A10 & A14 | 8 SQM UNIT A11 & A15 | 10.4 SQM UNIT B11 & B15 | 7.1 SQM UNIT B12 & B16 | 8 SQM UNIT B13 & B17 | 8 SQM UNIT B14 & B18 | 10.4 SQM



16.11.21 RC700

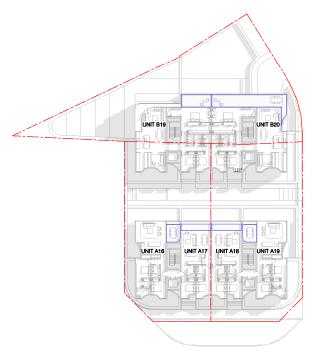
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KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

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PLANNING - OUTDOOR LIVING



3 OUTDOOR - LEVEL 5

DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT LEVEL 5

UNIT A16 | 10.4 SQM

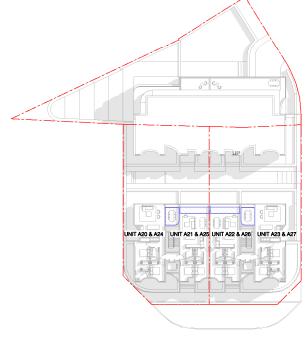
UNIT A17 | 8 SQM

UNIT A18 | 8 SQM

UNIT A19 | 10.4 SQM

UNIT B19 | 16.5 SQM UNIT B20 | 44.7 SQM

MONK MACKENZIE.



1 OUTDOOR - LEVEL 6 & LEVEL 7

DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT LEVEL 6 & 7

UNIT A20 & A24 | 10.4 SQM

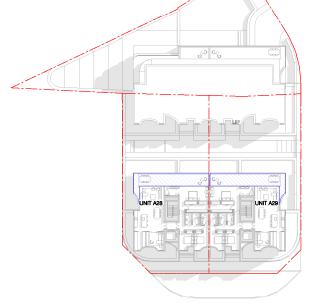
UNIT A21 & A25 | 8 SQM

UNIT A22 & A26 | 8 SQM UNIT A23 & A27 | 10.4 SQM

2 OUTDOOR - LEVEL 8 DIAGRAMS DEPICTING ACTUAL AREA AND DIMENSION OF OUTDOOR LIVING SPACE PROOVIDED AT LEVEL 8

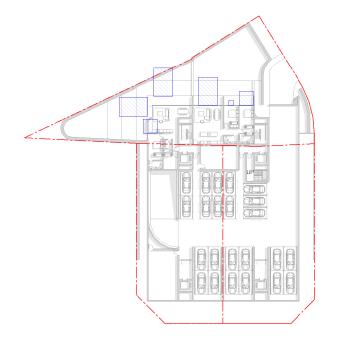
UNIT A28 | 44.7 SQM

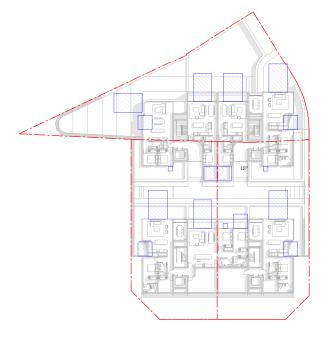
UNIT A29 | 44.7 SQM

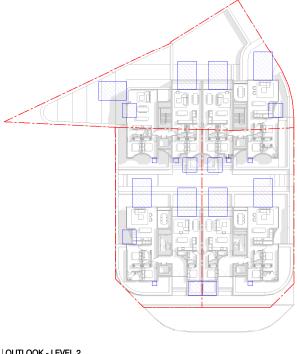


DRAFT

CONCEPT DESIGN PLANNING - OUTDOOR LIVING RC701 16.11.21 ALL CONSULTANTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, SITE MEASUREM AND CONDITIONS BEFORE ANY FABRICATION OR CONSTRUCTION BEGINS. COPYRIGHT OF THESE DRAWINGS IS THE PROPERTY OF MONK MACKENZIE ARCHITECTS LTD.



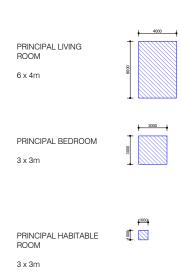






1 | OUTLOOK - BASEMENT | OUTLOOK - LEVEL 2 | OUTLOOK - LEVEL 3 & LEVEL 4 |
2 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
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3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 & LEVEL 4 |
3 | OUTLOOK - LEVEL 3 |
4 | OUTLOOK - LEVEL 3 |
5 | OUT

DIAGRAMS DEPICTING PRINCIPAL DIMENSION OF ROOM OUTLOOK REQUIRED



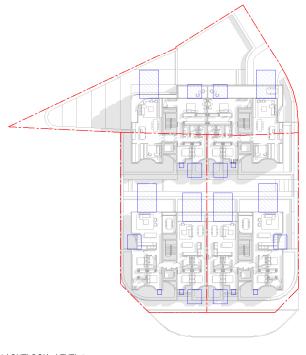
MONK MACKENZIE.

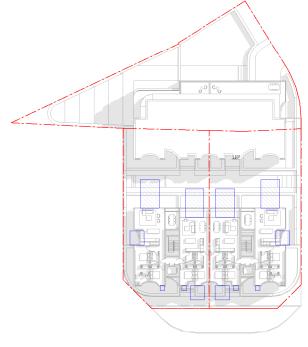
DRAFT

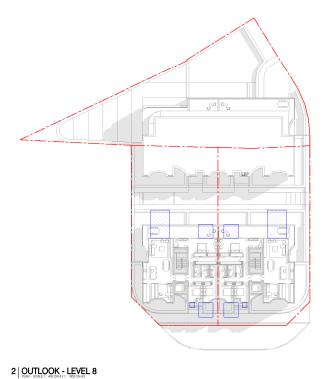
LEVEL 3, 23 O'CONNELL STREET

AUGKLAND, NEW ZEALAND
MONKMACKENZIE, COM
+ 649 9600 3335*
CUENT:

| LEVEL 3, 23 O'CONNELL STREET
| LEVEL 3, 24 O'CONNELL STRE

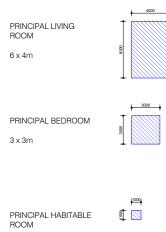






1 OUTLOOK - LEVEL 6 & LEVEL 7 3 OUTLOOK - LEVEL 5

DIAGRAMS DEPICTING PRINCIPAL DIMENSION OF ROOM OUTLOOK REQUIRED



3 x 3m

DRAFT

LEVEL 3, 23 O'CONNELL STREET
AUCKLAND, NEW ZEALAND
MONKMACKENZIE, COM
46 9600 3335

CLIENT NAME 182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND CONCEPT DESIGN KEPA ROAD APARTMENTS PLANNING - OUTLOOK RC703 16.11.21 ALL CONSULTANTS AND CONTRACTORS TO VERIFY ALL DIMENSIONS, ANGLES, SITE MEASUREM AND CONDITIONS BEFORE ANY FABRICATION OR CONSTRUCTION BEGINS. COPYRIGHT OF THESE DRAWINGS IS THE PROPERTY OF MONK MACKENZIE ARCHITECTS LTD.





1 | PLANNING - ALTERNATE HIRB

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CONCEPT DESIGN PLANNING - HIRB RC705 16.11.21



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KEPA ROAD APARTMENTS

182 & 184 KEPA ROAD , 8 KURAHAUPO STREET, AUCKLAND

CONCEPT DESIGN

VISUALIZATION - 3D MODEL SHOT

16.11.21 RC900



DRAFT



APPENDIX 2:

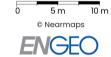
Investigation Location Plan





- Site Boundary
- Hand Auger Boreholes
- Machine Boreholes

- Contours 025m
- --- A-A' cross section
- --- B-B' Cross section



Title: Investigation Location Plan

Client: Sanctum Projects L				
Project: 182-184 Kepa Road, Orakei	Drawn: JC	Figure No: 1		
Date: 18-11-2021	Checked: PF	Size: A4		
Proj No: 19375.000.001	Scale: 1:565	Version: REV0		



APPENDIX 3:

Machine Borehole Logs





Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Client Ref. : 19375.000.001 Date : 20/10/2021 Hole Depth: 5 m

Logged By: JT Reviewed By: GC Latitude: -36.86134

Shear Vane No: 1546

Longitude: 174.82568 Hole Diameter: 50 mm Undrained Shear Strength (kPa) Peak/Remolded Graphic Symbol Elevation (mRL Symbol Depth (m BGL) Moisture Cond. Shear Vane Consistency/ Density Index Scala Penetrometer **Nater Level DESCRIPTION** Material USCS : Blows per 100mm 6 8 12 [TOPSOIL] Clayey SILT with minor rootlets; **TOPSOIL** brown. Low plasticity. Н OL 57.0 UTP Clayey SILT with trace sand; orange brown. Low 0.5 198+ -56.5 185/49 0.9 m - Becomes brown with dark brownish 1.0orange streaks. VSt-H ML 1.1 m - Becomes brown with brownish orange FIEL 157/68 streaks -56.0 **AUCKLAND VOLCANIC** Μ 1.5 198+ 1.65 m - Becomes reddish brown with trace 55.5 **UTP** Clayey SILT with trace sand; orange with light 2.0 grey streaks. Low plasticity. 175/66 VSt-H MI -55.0 143/54 2.4 m - Becomes intermixed orange and light 2.5 68/37 GEOTECH HAND AUGER HA01-05 SP01-05 MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 Clayey SILT with minor fine to medium sand; St ML -54.5 reddish brown. Low plasticity. Clayey SILT; greyish brown. Low plasticity. F 42/28 W -54.0 79/37 3.3 m - Becomes saturated. 3.5 -**PUKETOKA FORAMTION** ML57/34 St -53.5 S 93/42 78/41 Clayey SILT with trace sand; brown. Low 53.0 St ML Clayey SILT; orange. Low plasticity. 4.5 UTP M Н 4.65 m - Becomes grey and saturated. -52.5 69/35 S St End of Hole Depth: 5 m Termination Condition: Target depth

Hand auger met target depth at 5 m.

Dip test showed standing groundwater at 3.8 m depth.

N/A = Not Assessed; UTP = Unable to Penetrate.

Elevations obtained from Auckland Council GeoMaps (AUK46).



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client : Sanctum Projects Ltd Client Ref. : 19375.000.001 Date : 20/10/2021 Hole Depth: 5 m

Shear Vane No: 1546 Logged By : JT Reviewed By: GC

Latitude : -36.86128 Longitude: 174.82567

			Takei, Auckiand	Hole De		50 mm				Lon		le : -36			
Depth (m BGL)	Material	USCS Symbol	DESCRIPTION		Graphic Symbol	Elevation (mRL)	Water Level	Moisture Cond.	Consistency/ Density Index	Shear Vane Undrained Shear Strength (kPa) Peak/Remolded	2		s per 1	100mm 1 100mm	ı
_	TS	OL	[TOPSOIL] Clayey SILT with mino brown. Low plasticity.	r rootlets; dark	17. 71.17. 74.18. 77	. <u>/</u> .			N/A						
- - 0.5 - -			Clayey SILT with trace sand; orang trace black streaks. Low plasticity.	ge brown with		56.5			St-H	UTP 99/34					
- - 1.0 			1.0 m - Becomes intermixed brown	and orange		-56.0 - -			VSt	110/47					
-	AUCKLAND VOLCANIC FIELD	ML	brown with black streaks. 1.15 m - Becomes orange brown viblack streaks.	_		- -55.5				UTP					
- 1.5 - -	VOLCAN					- - -		М	н	UTP					
- - 2.0—	CKLAND		1.75 m - Becomes orange brown v brownish grey streaks.	vith trace light		-55.0 - -				UTP					
_ _ _	AU		Clayey SILT; orange brown with lig dark reddish orange streaks. Low	ght grey and plasticity.		-54.5				UTP		:			
- 2.5 - - - -			2.6 m - Becomes intermixed light orange.	grey and		- - - -54.0			VSt-H	UTP 198+					
- 3.0 -			Clayey SILT; greyish brown. Low p 2.90 m - becomes wet.			-				126/37					
-			3.1 m - Becomes greyish brown w mottles. 3.25 m - Becomes greyish brown.	ith black		- -53.5				71/21					
3.5 - - -	MTION	ML				-53.0		w	St-VSt	151/31					
- 4.0—	PUKETOKA FORAM					-				89/45					
_	UKETO		4.2 m - Becomes saturated.			- -52.5				UTP					
4.5 - - -	"					-	Ţ	S	н	UTP					
-			4.85 m - Becomes orange and mo	ist.		-52.0 -		М		UTP	:				
5.0 -			End of Hole Depth: 5 m Termination Condition: Target dep	th											
Dip N/A	o test A = N	show lot As	net target depth at 5 m. red standing groundwater at 4.5 m c sessed; TS = Topsoil; UTP = Unabl tained from Auckland Council GeoN	e to Penetrate.			Coc	ordina	tes obtai	ned from Arc	GIS (Collect	or.		



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client : Sanctum Projects Ltd Client Ref. : 19375.000.001 Date: 19/10/2021

Logged By : JT Reviewed By : GC Latitude : -36.86123

Shear Vane No: 1546

Hole Depth: 5 m Longitude: 174.82592 Hole Diameter : 50 mm

			Hole Diam	T								gituc						
BGL)		Symbol	DECORUDION		symbo		(mRL	vel	Cond.	ncy/	Vane d Shean n (KPa) molde	Scala Penetrometer						
Depth (m BGL)	Material	USCS S)	DESCRIPTION		Graphic Symbol	1	Elevation (mRL)	Water Level	Moisture Cond.	Consistency/ Density Index	Shear Vane Undrained Shear Strength (kPa) Peak/Remolded	2			per	100 8	mm 10	
		ML	[FILL] Clayey SILT with minor fine to medium sand; intermixed brown, grey and orange. Low plasticity. 10.1 m - Becomes brown.	XXXX		× × ×				N/A	62/30							
- 0.5 - - -	FILL	ML	Clayey SILT with minor fine to medium sand; dark brown with dark grey mottles. Low plasticity. 0.4 m - Becomes brown.			× × ×	- -55.5 -			St	51/20							
- - 1.0 -			Clayey SILT; brownish orange. Low plasticity.			Ĩ	- -55.0				UTP							
- - -			1.1 m - Becomes brownish orange with black streaks and trace sand.				-		М		UTP							
- 1.5 - -	AUCKLAND VOLCANIC FIELD	ML					- -54.5			Н	UTP							
- - 2.0	VOLCAN		1.8 m - Becomes orange.				- - 54.0				UTP							
0 -	LAND	_ML_	Clayey SILT with trace medium sand; reddish brown with orange streaks. Low plasticity.			t	-			Н	UTP		:		:			
- - 2.5 -		ML	Clayey SILT with trace sand; intermixed light grey and orange with black streaks. Low plasticity.				- - -53.5			н	UTP							
			2.6 m - Becomes brownish grey and wet.				Ė		w		161/31							
3.0		ML	Clayey SILT with minor fine to medium sand; reddish brown. Low plasticity.	_		+	- -53.0			VSt	57/28							
- - -			Clayey SILT; brownish grey. Low plasticity.				-	_		F-St	47/31							
- 3.5 - -	MTION						- -52.5 -	Ţ			UTP							
- - 4 0	FORAMT	ML					- - -52.0		S	St-H	66/34							
- - -	PUKETOKA FORA	IVIL					-				UTP							
- 4.5 - -	PU		4.4 m - Becomes intermixed grey and orange. 4.55 m - Becomes orange.				- -51.5 -			н	UTP							
- - 5.0			4.9 m - Becomes grey.				51.0				UTP							
_			End of Hole Depth: 5 m Termination Condition: Target depth				01.0								<u>:</u>			
Dip N/A	test A = N	show lot As	net target depth at 5 m. red standing groundwater at 3.4 m depth. sessed; UTP = Unable to Penetrate. tained from Auckland Council GeoMaps (AUK46).					Coc	ordina	ates obtai	ned from Arc	GIS	Colle	∍cto	r.			



Coordinates obtained from Arc GIS Collector.

Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Client Ref. : 19375.000.001 Date : 19/10/2021 Hole Depth: 5 m

Hole Diameter: 50 mm

Logged By: JT Reviewed By: GC Latitude : -36.86102 Longitude: 174.82547

Shear Vane No: 1546

Undrained Shear Strength (kPa) Peak/Remolded Graphic Symbol Elevation (mRL Symbol Depth (m BGL) Moisture Cond. Shear Vane Consistency/ Density Index Scala Penetrometer **Nater Level** DESCRIPTION Material USCS : Blows per 100mm 6 8 10 12 [TOPSOIL] Clayey SILT with minor rootlets; dark OL N/A 54.5 brown. Low plasticity. Clayey SILT with trace sand; brown with orange 96/34 mottles. Low plasticity. 0.5 54.0 155/35 St-H 181/78 0.9 m - Becomes orange brown. 1.0-AUCKLAND VOLCANIC FIELD 1.0 m - Becomes dark orange brown with trace -53.5 black streaks. **UTP** M 1.5 UTP 53.0 Clayey SILT with minor fine to medium sand; orange with light grey streaks. Low plasticity. **UTP** ML2.0-Clayey SILT with trace medium sand; brownish red. Low plasticity. 52.5 2.15 m - Becomes intermixed orange and light VSt-H ML 2.4 m - Becomes brownish red with black 2.5 streaks, -52.0 Clayey SILT; intermixed light grey and orange ML with trace black streaks. Low plasticity. GEOTECH HAND AUGER HA01-05 SP01-05 MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 Clayey SILT with minor fine to medium sand; Н brownish red with red streaks. Low plasticity 3.0 54/31 Clayey SILT with trace sand; greyish brown with -51.5 occasional brownish red laminations. Low plasticity. 187/25 W 3.5 -PUKETOKA FORAMTION 51.0 107/37 3.7 m - Becomes saturated. 59/28 St-H ML -50.5 96/31 S 4.5 UTP 50.0 4.6 m - Becomes dark greyish brown with black streaks. UTP 4.7 m - Becomes orange. End of Hole Depth: 5 m Termination Condition: Target depth

Hand auger met target depth at 5 m.

Dip test showed standing groundwater at 3.6 m depth.

N/A = Not Assessed; T = Topsoil; UTP = Unable to Penetrate.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Client Ref. : 19375.000.001 Date : 19/10/2021 Hole Depth: 5 m

Logged By: JT Reviewed By: GC Latitude : -36.86096

Shear Vane No: 1546

Longitude: 174.82586 Hole Diameter: 50 mm Undrained Shear Strength (kPa) Peak/Remolded Graphic Symbol Elevation (mRL Symbol Depth (m BGL) Moisture Cond. Shear Vane Consistency/ Density Index Scala Penetrometer **Nater Level DESCRIPTION** Material USCS : Blows per 100mm 6 8 10 12 [TOPSOIL] Clayey SILT with minor rootlets; dark 2 brown. Low plasticity. N/A OL 53.0 Clayey SILT with trace sand; brown with 102/37 occasional orange mottles. Low plasticity. 0.5 UTP 0.7 m - Becomes orange brown. 52.5 **UTP** 1.0 1.0 m - Becomes intermixed brown and orange VSt-H brown with black streaks. **UTP** 52.0 M 1.5 **UTP** AUCKLAND VOLCANIC 51.5 **UTP** Clayey SILT with minor fine sand; intermixed 2.0 reddish brown and orange brown with brownish **UTP** grey spots. Low plasticity. Н ML 51.0 UTP Clayey SILT; intermixed light grey and orange. 2.5 Low plasticity. 171/68 GEOTECH HAND AUGER HA01-05 SP01-05 MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 -50.5 2.85 m to 2.9 m - Encountered layer of clayey St-H ML SILT with some fine to coarse sand; intermixed 3.0 123/37 black, grey and orange. Low plasticity. 2.9 m - Becomes wet. W 3.0 m - Becomes greyish brown. 50.0 85/34 Clayey SILT with minor fine sand; reddish 3.5 brown. Low plasticity. 59/30 3.5 m - Becomes saturated. 49.5 PUKETOKA FORMATION 52/40 153/27 F-H ML 49.0 S 4.5 UTP 48.5 4.7 m - Becomes orange. 42/25 4.85 m - Becomes grey. End of Hole Depth: 5 m

Hand auger met target depth at 5 m.

Dip test showed standing groundwater at 4.1 m depth.

N/A = Not Assessed; TS = Topsoil; UTP = Unable to Penetrate.

Termination Condition: Target depth

Elevations obtained from Auckland Council GeoMaps (AUK46).



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Logged By/Reviewed By: KW / JC Drilling Method: Rotosonic Latitude : -36.86135 19375.000.001 Drilling Contractor: Prodrill Ltd Longitude: 174.82557 Depth (m BGL) Shear JSCS Symbol Elevation (mRL Consistency/ Density Index Sample Type Log Symbol Water Level **Total Core** SPT **DESCRIPTION** Torvane ((kPa) Recovery Moisture Notes Material N-Value (%) [ASPHALT] ᆵ N/A [CONCRETE] N/A Clayey SILT with some fine to coarse gravel; brown with orange and black streaks and mottles. Low plasticity. 0.5 GP Encountered trace rootlets between 0.25 m and 49/25 ML 0.65 m (< 2 mm diameter). Fine to medium GRAVEL; dark brown with red and black clasts. Poorly graded. NO RECOVERY. 1.0-57 F Clayey SILT with trace fine to medium SAND; 34/17 intermixed grey and orange. Low plasticity. MLClayey SILT; dark brown. Low plasticity. 1.5 Н 1/1/2/2/3/4 N=11 Silty CLAY with trace fine to medium sand; 2.0 UTP intermixed grey and orange. High plasticity. М N/A Encountered dark brown sand with dark red and black clasts lens' at 2.0 m, 2.05 m, 2.15 m and Ⅱ 2.20 m. Silty CLAY; grey and orange. High plasticity. Encountered dark brown sand with dark red and **AUCKLAND VOLCANIC** 2.5 97/42 MACHINE BORING HA01-05_SP01-05_MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 black clasts lens' at 2.37 m, 2.50 m, 2.55 m, 2.60 m and 2 90 m Clayey SILT; light grey with some light brown 3.0--55 streaks. Low plasticity. N/A 0/0/0/0/0/0 3.5 s -54 4.5 80/11 W 0/0/1/0/1/2 N=4 5.0 4.95 m - encountered sand lens; dark brown with dark red and black clasts. N/A

Coordinates obtained from Arc GIS Collector.

SEOTECH

Dip test showed standing groundwater at 3.95 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road

Client: Sanctum Projects Ltd Core Diameter: 83 mm Date: 19/10/2021 Energy Transfer Ratio: 80.3 %

VW

Orakei, Auckland Hole Depth: 19.65 m Logged By/Reviewed By: KW / JC Drilling Method: Rotosonic Latitude : -36.86135 19375.000.001 Drilling Contractor: Prodrill Ltd Longitude: 174.82557 Depth (m BGL) Shear **USCS Symbol** Elevation (mRL Consistency/ Density Index Sample Type Log Symbol Water Level **Total Core** SPT **DESCRIPTION** Recovery Moisture Torvane ((kPa) Notes Material N-Value (%) Clayey SILT; brownish orange. Low plasticity. Silty CLAY; dark grey. High plasticity. **PUKETOKA FORMATION** Encountered trace black streaks of amorphous 5.5 organics between 5.2 m and 5.4 m. 5.4 m - encountered partially decomposed wood fragments (20 mm diameter). 5.55 m - becomes grey with minor orange streaks. Encountered trace black streaks of amorphous S organics between 5.65 m and 5.75 m. 6.0 31/14 0/0/0/0/0/0 N=0 Silty CLAY; bluish grey with brownish orange 6.5 streaks. High plasticity. 7.5 W 59/30 0/0/0/1/2/1 N=4 GEOTECH MACHINE BORING HA01-05 SP01-05 MBH01-03 - COPY GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 7.85 m - becomes grey. BAYS FORMATION 8.0-F-St 8.5 EASTCOAST 8.90 m - encountered 100 mm dark blackish grey 9.0layer. UTP 2/2/3/4/4/5 N=17 9.5 UTP Highly weathered, intermixed grey and dark grey SILTSTONE; very weak. VW 10.0 Highly weathered, intermixed grey and dark grey fine SANDSTONE; very weak. VW

Coordinates obtained from Arc GIS Collector.

Dip test showed standing groundwater at 3.95 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Core Diameter: 83 mm Date: 19/10/2021 Energy Transfer Ratio: 80.3 % Hole Depth: 19.65 m

Logged By/Reviewed By: KW / JC Latitude : -36.86135

19375.000.001

Drilling Method: Rotosonic Drilling Contractor: Prodrill Ltd

Longitude: 174.82557 Depth (m BGL) Shear JSCS Symbol Elevation (mRL Consistency/ Density Index Sample Type Log Symbol Water Level **Total Core** SPT **DESCRIPTION** Recovery Moisture Torvane ((kPa) Notes Material N-Value (%) 50 Highly weathered, intermixed grey and dark grey XXXXXXXXXXXXXXXXXXXXXX 10.5 SIĽTŠTONE; very weak. 3/4/5/6/8/11 N=30 11 0 VW 11.5 Highly weathered, intermixed grey and dark grey VW fine SANDSTONE; very weak *********** Highly weathered, intermixed grey and dark grey SILTSTONE; very weak. 46 12.0 7/17/50 N=50 BAYS FORMATION 12.5 VW 3EOTECH MACHINE BORING HA01-05_SP01-05_MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 13.0 EASTCOAST 13.5 3/5/25/25 Highly weathered, intermixed grey and dark grey 14.0 fine SANDSTONE; very weak. VW Highly weathered, intermixed grey and dark grey SILTSTONE; very weak. 14.5 XXXXXXXXXXXXXXXXX 44/6 15.0 VW 15.5

Coordinates obtained from Arc GIS Collector.

Dip test showed standing groundwater at 3.95 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd
Date: 19/10/2021

Banche: 19.65 m

Ltd Core Diameter: 83 mm Energy Transfer Ratio: 80.3 % Logged By/Reviewed By: KW / JC

Hole Depth: 19.65 m
Drilling Method: Rotosonic
Drilling Contractor: Prodrill Ltd

Latitude : -36.86135 Longitude : 174.82557

19375.000.001

Depth (m BGL) Shear **USCS Symbol** Elevation (mRL Consistency/ Density Index Sample Type Log Symbol Water Level **Total Core** SPT Moisture **DESCRIPTION** Torvane ((kPa) Recovery Notes Material N-Value (%) VWHighly weathered, intermixed grey and dark grey **** fine SANDSTONE; very weak. Highly weathered, intermixed grey and dark grey SILTŠTONE; very weak. 16.0 42 VW Highly weathered, intermixed grey and dark grey fine SANDSTONE; very weak. VW 16.5 50 Highly weathered, intermixed grey and dark grey XXXXXXXX N=50 SILTSTONE; very weak. VW 17.0 Highly weathered, intermixed grey and dark grey EASTCOAST BAYS FORMATION fine SANDSTONE; very weak. VW Highly weathered, intermixed grey and dark grey XXXXXXXXXXXXXXX SILTSTONE; very weak. 17.5 VW 40/10 18.0 40 Highly weathered, intermixed grey and dark grey fine SANDSTONE; very weak. **\/\/** 18.5 Highly weathered, intermixed grey and dark grey xxxxxxxxxxxxx SILTSTONE; very weak. 19.0 39 VW 19.5 35/15 N=50

End of Hole Depth: 19.65 m Termination: Target depth

Coordinates obtained from Arc GIS Collector.

3EOTECH MACHINE BORING HA01-05_SP01-05_MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21

Dip test showed standing groundwater at 3.95 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Date: 20/10/2021 Hole Depth: 18.05 m Drilling Method: Rotosonic

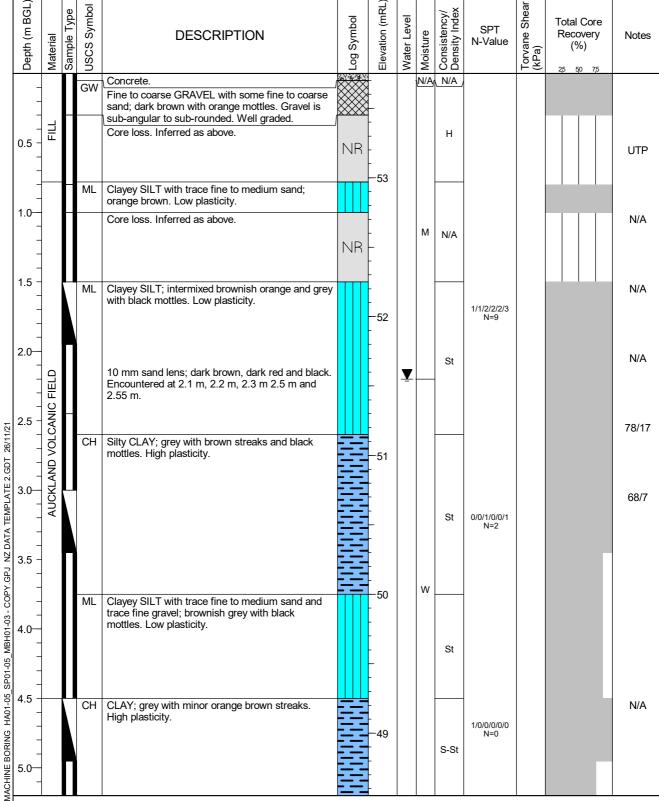
Core Diameter: 83 mm Energy Transfer Ratio: 80.3 % Logged By/Reviewed By: KW / JC

Latitude : -36.86102 Longitude: 174.82586

19375.000.001

Shear Elevation (mRL Consistency/ Density Index Log Symbol Water Level **Total Core** SPT Moisture **DESCRIPTION** Torvane ((kPa) Recovery Notes N-Value (%) N/A N/A

Drilling Contractor: Prodrill Ltd



Coordinates obtained from Arc GIS Collector.

SEOTECH

Dip test showed standing groundwater at 2.2 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Date: 20/10/2021

Core Diameter: 83 mm Energy Transfer Ratio : 80.3~% $\textbf{Logged By/Reviewed By} : \mathsf{KW} \ / \ \mathsf{JC}$

Hole Depth: 18.05 m Drilling Method : Rotosonic

Latitude : -36.86102 19375.000.001 Drilling Contractor: Prodrill Ltd Longitude: 174.82586 Depth (m BGL) Shear **USCS Symbol** Elevation (mRL Consistency/ Density Index Sample Type Log Symbol Water Level **Total Core** SPT **DESCRIPTION** Torvane ((kPa) Recovery Moisture Notes Material N-Value (%) CLAY; grey with minor orange brown streaks. High plasticity. 5.5 PUKETOKA FORMATION 6.0 31/10 0/0/1/1/1/1 N=4 S-St 6.5 W 7.5 CLAY; grey with some orange brown streaks. 71/11 High plasticity. 1/1/2/2/2/2 N=8 GEOTECH MACHINE BORING HA01-05 SP01-05 MBH01-03 - COPY GPJ NZ DATA TEMPLATE 2.GDT 26/11/21 St-H BAYS FORMATION 8.5 82/24 UTP Clayey SILT: interbedded brown and dark grey. 5/19/17/17/16 COAST Non-plastic. [Highly weathered, externely weak N=50 SILTSTONE]. Highly weathered interbedded light and dark grey EAST SILTSTONE; very weak. 9.5 -VW 10.0

Coordinates obtained from Arc GIS Collector.

Dip test showed standing groundwater at 2.2 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Core Diameter: 83 mm Date: 20/10/2021 Energy Transfer Ratio : 80.3~%Hole Depth: 18.05 m $\textbf{Logged By/Reviewed By} : \mathsf{KW} \ / \ \mathsf{JC}$

	Drilling Method: Rotosonic 19375.000.001 Drilling Contractor: Prodrill Ltd						Latitude : -36.86102 Longitude : 174.82586							
Depth (m BGL)	Material	Sample Type	USCS Symbol	DESCRIPTIO		og Symbol	Elevation (mRL)	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
10.5				Core loss from SPT.		NR	- - 43			vw	11/15/31/19 N=50			
11.0		n		Highly weathered, interbedded l grey SILTSTONE; very weak.	ight grey and dark	× × × × × × × × × × × × × × × × × × ×	- - -			VW				
-				Highly weathered, grey and dark SANDSTONE; very weak, lamir	nated.		-			VW				
11.5				Highly weathered, interbedded I grey SILTSTONE; very weak.		× × × × × × × × × × × × × × × × × × ×	_			VW				
12. 0				Highly weathered, grey and dark SANDSTONE; very weak, lamin in c.200 mm layers with highly interbedded light grey and dark very weak.	nated. Interbedded weathered,	/ × × × × × × × × × × × × × × × × × × ×					9/18/50 N=50			
12.5 13. 0 13. 0	S FORMATI					X X X X X X X X X X X X X X X X X X X	- - - -41 - - -							
-03 - COPY GPJ NZ DATA TEMPLATE 2: GDT 26/11/21	EAST					× × × × × × × × × × × × × × × × × × ×				vw	35/15 N=50			
14.0-14.5-14.0-109-109-109-109-109-109-109-109-109-10						X X X X X X X X X X X X X X X X X X X	- - -39 - - - - -				23/27 N=50			

Coordinates obtained from Arc GIS Collector.

Dip test showed standing groundwater at 2.2 m depth at 15:30 18/11/2021.



Geotechnical Investigation 182-184 Kepa Road Orakei, Auckland

Client: Sanctum Projects Ltd Core Diameter: 83 mm Date: 20/10/2021 Energy Transfer Ratio : 80.3~%Hole Depth: 18.05 m $\textbf{Logged By/Reviewed By} : \mathsf{KW} \ / \ \mathsf{JC}$ **Latitude**: -36.86102

Drilling Method: Rotosonic Drilling Contractor: Prodrill Ltd

Longitude: 174.82586

	19375.000.001 Drilling Contractor : Prodrill Ltd Longitude : 174.82586						86							
Depth (m BGL)	Material	Sample Type	_	DESCRIPTION		Log Symbol	Elevation (mRL)	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
16. 0	EAST COAST BAYS FORMATION			Highly weathered, grey and dark SANDSTONE; very weak, lamin in c.200 mm layers with highly interbedded light grey and dark very weak.	k grey fine nated. Interbedded weathered, grey SILTSTONE;	X X X X X X X X X X X X X X X X X X X	- - - - - - - - - - - - - - - -			> W	13/37 N=50			

End of Hole Depth: 18.05 m Termination: Target depth

Coordinates obtained from Arc GIS Collector.

Dip test showed standing groundwater at 2.2 m depth at 15:30 18/11/2021. Elevations obtained from Auckland Council GeoMaps (AUK46).

SEOTECH MACHINE BORING HA01-05_SP01-05_MBH01-03 - COPY.GPJ NZ DATA TEMPLATE 2.GDT 26/11/21



Figure 1: 0.00 m – 2.80 m



Figure 2: 2.80 m – 6.45 m



MBH01 Core Photos

Client: Sanctum Projects Ltd					
Project: 182 Kepa Road, Orakei	Drawn: JCh	Page No: 1 Size: A4			
Date: 20/10/2021	Checked: KW	OIZC. AT			
Proj No: 19375.000.001	Scale: NTS	Revision: 01			



Figure 3: 6.45 m – 9.75 m



Figure 4: 9.75 m – 13.50 m



MBH01 Core Photos

Client: Sanctum Projects Ltd		
Project: 182 Kepa Road, Orakei	Drawn: JCh	Page No: 2 Size: A4
Date: 20/10/2021	Checked: KW	Size. A4
Proj No: 19375.000.001	Scale: NTS	Revision: 01



Figure 5: 13.50 m – 16.87 m



Figure 6: 16.87 m - 19.50 m



MBH01 Core Photos

Client: Sanctum Projects Ltd					
Project: 182 Kepa Road, Orakei	Drawn: JCh	Page No: 3 Size: A4			
Date: 20/10/2021	Checked: KW	OIZC. AT			
Proj No : 19375.000.001	Scale: NTS	Revision: 01			



Figure 1: 0.00 m – 3.75 m



Figure 2: 3.75 m – 7.12 m



MBH02 Core Photos

Client: Sanctum Projects Ltd					
Project: 182 Kepa Road, Orakei	Drawn: JCh	Page No: 1 Size: A4			
Date: 20/10/2021	Checked: KW	OIZC. AT			
Proj No: 19375.000.001	Scale: NTS	Revision: 01			



Figure 3: 7.12 m – 10.40 m



Figure 4: 10.40 m - 13.90 m



MBH02 Core Photos

Client: Sanctum Projects Ltd						
Project: 182 Kepa Road, Orakei	Drawn: JCh	Page No: 2 Size: A4				
Date: 20/10/2021	Checked: KW	OIZC. AT				
Proj No: 19375.000.001	Scale: NTS	Revision: 01				



Figure 5: 13.90 m – 17.53 m



Figure 6: 17.53 m - 18.00 m



MBH02 Core Photos

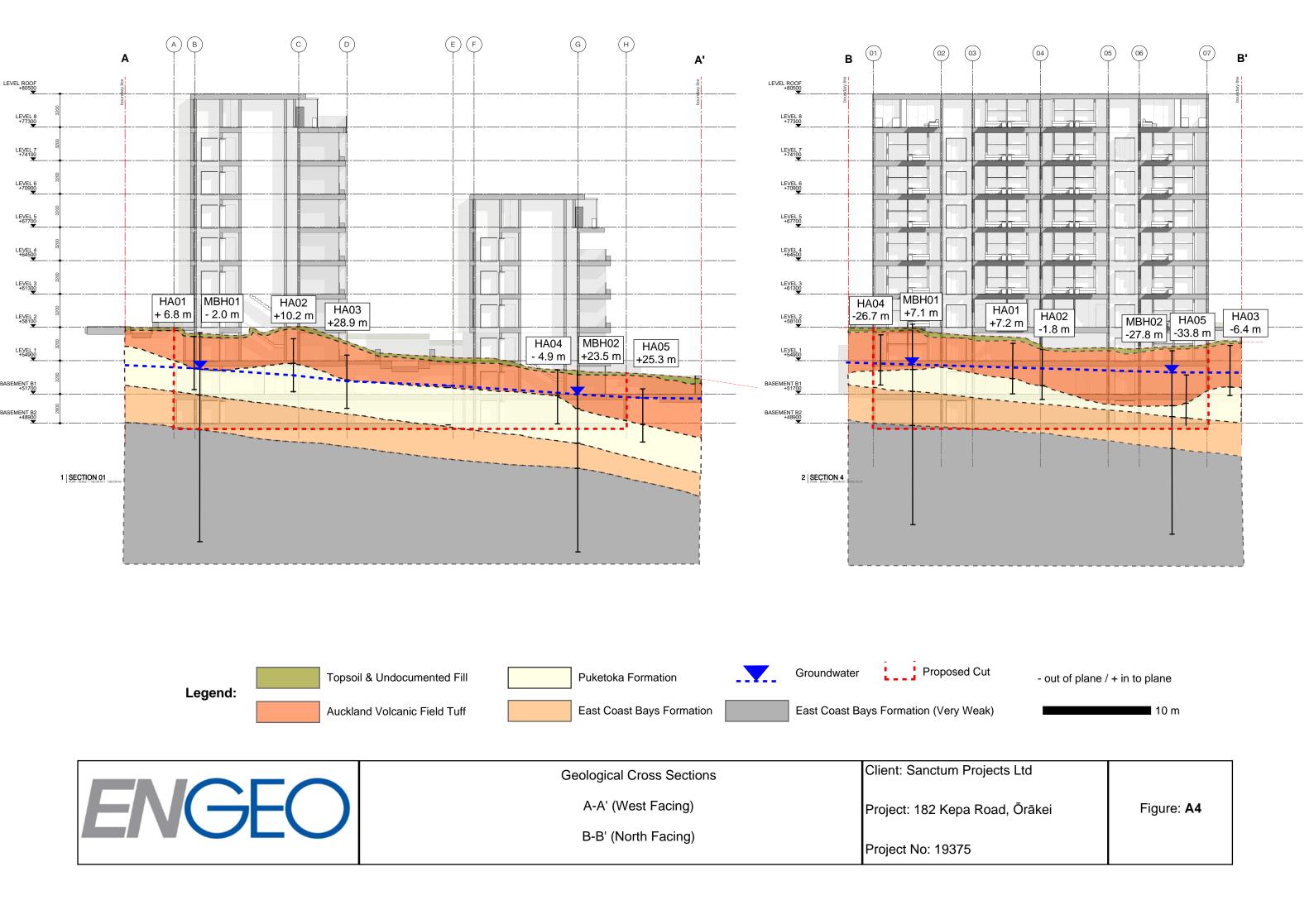
Client: Sanctum Projects Ltd						
Project: 182 Kepa Road, Orakei	Drawn: JCh	Page No: 3 Size: A4				
Date: 20/10/2021	Checked: KW	OIZC. AT				
Proj No : 19375.000.001	Scale: NTS	Revision: 01				



APPENDIX 4:

Interpretive Ground Model







APPENDIX 5:

Groundwater Monitoring Data



